# 14.5 Limitation on Liability

- 14.5.1 Except as expressly provided in this Agreement, neither the TSP nor the Nodal Agency nor their respective officers, directors, agents, employees or Affiliates (including, officers, directors, agents or employees of such Affiliates), shall be liable or responsible to the other Party or its Affiliates including its officers, directors, agents, employees, successors, insurers or permitted assigns for incidental, indirect or consequential, punitive or exemplary damages, connected with or resulting from performance or non-performance of this Agreement, or anything done in connection herewith, including claims in the nature of lost revenues, income or profits (other than payments expressly required and properly due under this Agreement), any increased expense of, reduction in or loss of transmission capacity or equipment used therefore, irrespective of whether such claims are based upon breach of warranty, tort (including negligence, whether of the Nodal Agency, the TSP or others), strict liability, contract, breach of statutory duty, operation of law or otherwise.
- 14.5.2 The Nodal Agency shall have no recourse against any officer, director or shareholder of the TSP or any Affiliate of the TSP or any of its officers, directors or shareholders for such claims excluded under this Article. The TSP shall also have no recourse against any officer, director or shareholder of the Nodal Agency, or any Affiliate of the Nodal Agency or any of its officers, directors or shareholders for such claims excluded under this Article.

# 14.6 Duty to Mitigate

The party entitled to the benefit of an indemnity under this Article 14 shall take all reasonable measures to mitigate any loss or damage which has occurred. If the Party fails to take such measures, the other Party's liabilities shall be correspondingly reduced.



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#### **ARTICLE: 15**

#### 15 ASSIGNMENTS AND CHARGES

#### 15.1 Assignments:

15.1.1 This Agreement shall be binding upon, and inure to the benefit of the Parties and their respective successors and permitted assigns. This Agreement shall not be assigned by any Party, except as provided in Article 15.3.

## 15.2 Permitted Charges:

- 15.2.1 Neither Party shall create or permit to subsist any encumbrance over all or any of its rights and benefits under this Agreement.
- 15.2.2 However, the TSP may create any encumbrance over all or part of the receivables, or the Project Assets of the Project in favour of the Lenders or the Lenders' Representative on their behalf, as security for amounts payable under the Financing Agreements and any other amounts agreed by the Parties.

#### Provided that:

- the Lenders or the Lenders' Representative on their behalf shall have entered into the Financing Agreements and agreed in writing to the provisions of this Agreement; and
- ii. any encumbrance granted by the TSP in accordance with this Article 15.2.2 shall contain provisions pursuant to which the Lenders or the Lender's Representative on their behalf agrees unconditionally with the TSP to release from such encumbrances upon payment by the TSP to the Lenders of all amounts due under the Financing Agreements.

## 15.2.3 Article 15.2.1 does not apply to:

- a. liens arising by operation of law (or by an agreement evidencing the same) in the ordinary course of the TSP developing and operating the Project;
- pledges of goods, the related documents of title and / or other related documents, arising or created in the ordinary course of the TSP developing and operating the Project; or
- c. security arising out of retention of title provisions in relation to goods acquired in the ordinary course of the TSP developing and operating the Project.

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# 15.3 Substitution Rights of the Lenders

- 15.3.1 The TSP would need to operate and maintain the Project under the provisions of this Agreement and cannot assign the Transmission License or transfer the Project or part thereof to any person by sale, lease, exchange or otherwise, without the prior approval of the Nodal Agency.
- 15.3.2 However, in the case of default by the TSP in debt repayments or in the case of default by the TSP as per Article 13 of this Agreement during the debt repayments, the Commission may, on an application from the Lenders, assign the Transmission License to the nominee of the Lenders subject to the fulfilment of the qualification requirements and provisions of the Central Electricity Regulatory Commission (Procedure, terms and Conditions for grant of Transmission License and other related matters) Regulations, 2006 and as amended from time to time.

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**ARTICLE: 16** 

#### 16 GOVERNING LAW AND DISPUTE RESOLUTION

#### 16.1 Governing Law:

This Agreement shall be governed by and construed in accordance with the Laws of India. Any legal proceedings in respect of any matters, claims or disputes under this Agreement shall be under the jurisdiction of appropriate courts in Delhi.

#### 16.2 Amicable Settlement:

- 16.2.1 Either Party is entitled to raise any claim, dispute or difference of whatever nature arising under, out of or in connection with this Agreement, including its existence or validity or termination or whether during the execution of the Project or after its completion and whether prior to or after the abandonment of the Project or termination or breach of the Agreement by giving a written notice to the other Party, which shall contain:
  - (i) a description of the Dispute;
  - (ii) the grounds for such Dispute; and
  - (iii) all written material in support of its claim.
- 16.2.2 The other Party shall, within thirty (30) days of issue of notice issued under Article 16.2.1, furnish:
  - (i) counter-claim and defences, if any, regarding the Dispute; and
  - (ii) all written material in support of its defences and counter-claim.
- 16.2.3 Within thirty (30) days of issue of notice by the Party pursuant to Article 16.2.1, if the other Party does not furnish any counter claim or defense under Article 16.2.2, or thirty (30) days from the date of furnishing counter claims or defence by the other Party, both the Parties to the Dispute shall meet to settle such Dispute amicably. If the Parties fail to resolve the Dispute amicably within thirty (30) days from the later of the dates mentioned in this Article 16.2.3, the Dispute shall be referred for dispute resolution in accordance with Article 16.3.

## 16.3 Dispute Resolution:

All Disputes shall be adjudicated by the Commission.

#### 16.4 Parties to Perform Obligations:

Notwithstanding the existence of any Dispute and difference referred to the Commission as provided in Article 16.3 and save as the Commission may otherwise direct by a final or interim order, the Parties hereto shall continue to perform their respective obligations/ roles (which are not in dispute) under this Agreement.

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**ARTICLE: 17** 

#### 17 REPRESENTATION AND WARRANTIES

# 17.1 Representation and warranties of the Nodal Agency

- 17.1.1 The Nodal Agency hereby represents and warrants to and agrees with the TSP as follows and acknowledges and confirms that the TSP is relying on such representations and warranties in connection with the transactions described in this Agreement:
  - a. It has all requisite powers and authority to execute and consummate this Agreement;
  - b. This Agreement is enforceable against the Nodal Agency in accordance with its terms;
  - c. The consummation of the transactions contemplated by this Agreement on the part of Nodal Agency will not violate any provision of nor constitute a default under, nor give rise to a power to cancel any charter, mortgage, deed of trust or lien, lease, agreement, license, permit, evidence of indebtedness, restriction, or other contract to which the Nodal Agency is a Party or to which the Nodal Agency is bound, which violation, default or power has not been waived;

## 17.2 Representation and Warranties of the TSP:

- 17.2.1 The TSP hereby represents and warrants to and agrees with the Nodal Agency as follows and acknowledges and confirms that the Nodal Agency is relying on such representations and warranties in connection with the transactions described in this Agreement:
  - a. It has all requisite powers and has been duly authorized to execute and consummate this Agreement;
  - This Agreement is enforceable against it, in accordance with its terms;
  - c. The consummation of the transactions contemplated by this Agreement on the part of the TSP will not violate any provision of nor constitute a default under, nor give rise to a power to cancel any charter, mortgage, deed of trust or lien, lease, agreement, license, permit, evidence of indebtedness, restriction, or other contract to which the TSP is a Party or to which the TSP is bound which violation, default or power has not been waived;

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- d. The TSP is not insolvent and no insolvency proceedings have been instituted, nor threatened or pending by or against the TSP;
- e. There are no actions, suits, claims, proceedings or investigations pending or, to the best of the TSP's knowledge, threatened in writing against the TSP at law, in equity, or otherwise, and whether civil or criminal in nature, before or by, any court, commission, arbitrator or governmental agency or authority, and there are no outstanding judgments, decrees or orders of any such courts, commission, arbitrator or governmental agencies or authorities, which materially adversely affect its ability to execute the Project or to comply with its obligations under this Agreement.
- 17.2.2 The TSP makes all the representations and warranties above to be valid as on the Effective Date of this Agreement.

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#### **ARTICLE: 18**

#### **18 INDEPENDENT ENGINEER**

## 18.1 Appointment of Independent Engineer

The Nodal Agency shall appoint an agency/ company as Independent Engineer as per framework provided in the Guidelines for Encouraging Competition in Development of Transmission Projects for selection of Independent Engineer.

# 18.2 Roles and functions of Independent Engineer

The role and functions of the Independent Engineer shall include the following:

- a. Progress Monitoring as required under this Agreement;
- b. Ensuring Quality as required under this Agreement;
- determining, as required under the Agreement, the costs of any works or services and/or their reasonableness during construction phase;
- d. determining, as required under the Agreement, the period or any extension thereof, for performing any duty or obligation during construction phase;
- e. determining, as required under the Agreement, the valuation of the Project Assets.
- f. Assisting the Parties in resolution of Disputes and
- g. Undertaking all other duties and functions in accordance with the Agreement.

## 18.3 Remuneration of Independent Engineer

The fee and charges of the Independent Engineer shall be paid by the Nodal Agency as per terms & conditions of appointment.

## 18.4 Termination of appointment

- 18.4.1 The Nodal Agency may, in its discretion, terminate the appointment of the Independent Engineer at any time, but only after appointment of another Independent Engineer.
- 18.4.2 If the TSP has reason to believe that the Independent Engineer is not discharging its duties and functions in a fair, efficient and diligent manner, it may make a written representation to the Nodal Agency and seek termination of the appointment of the Independent Engineer. Upon receipt of such representation, the Nodal Agency shall

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hold a tripartite meeting with the TSP and Independent Engineer for an amicable resolution, and the decision of Nodal agency is final. In the event that the appointment of the Independent Engineer is terminated hereunder, the Nodal Agency shall appoint forthwith another Independent Engineer.

## 18.5 Authorised signatories

The Nodal Agency shall require the Independent Engineer to designate and notify to the Nodal Agency up to 2 (two) persons employed in its firm to sign for and on behalf of the Independent Engineer, and any communication or document required to be signed by the Independent Engineer shall be valid and effective only if signed by any of the designated persons; provided that the Independent Engineer may, by notice in writing, substitute any of the designated persons by any of its employees.



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**ARTICLE: 19** 

#### 19 MISCELLANEOUS PROVISIONS

#### 19.1 Equity Lock-in Commitment:

19.1.1 The aggregate equity share holding of the Selected Bidder in the issued and paid up equity share capital of "MUNDRA I TRANSMISSION LIMITED" shall not be less than Fifty one percent (51%) up to a period of one (1) year after COD of the Project.

Provided that, in case the Lead Member or Bidding Company is holding equity through Affiliate/s, Ultimate Parent Company or Parent Company, such restriction as specified above shall apply to such entities.

Provided further, that in case the Selected Bidder is a Bidding Consortium, the Lead Member shall continue to hold equity of at least twenty six percent (26%) upto a period of one (1) year after COD of the Project and any Member of such Bidding Consortium shall be allowed to divest its equity as long as the other remaining Members (which shall always include the Lead Member) hold the minimum equity specified above.

- 19.1.2 If equity is held by the Affiliates, Parent Company or Ultimate Parent Company of the Selected Bidder, then, subject to the second proviso to Article 19.1.1, such Affiliate, Parent Company or Ultimate Parent Company shall be eligible to transfer its shareholding in "MUNDRA I TRANSMISSION LIMITED" to another Affiliate or to the Parent Company / Ultimate Parent Company of the Selected Bidder. If any such shareholding entity, qualifying as an Affiliate / Parent Company / Ultimate Parent Company, is likely to cease to meet the criteria to qualify as an Affiliate / Parent Company / Ultimate Parent Company / Ultimate Parent Company of the Selected Bidder.
- 19.1.3 Subject to Article 19.1.1, all transfer(s) of shareholding of "MUNDRA I TRANSMISSION LIMITED" by any of the entities referred to in Article 19.1.1 and 19.1.2 above, shall be after prior written intimation to the Nodal Agency.
- 19.1.4 For computation of effective Equity holding, the Equity holding of the Selected Bidder or its Ultimate Parent Company in such Affiliate(s) or Parent Company and the equity holding of such Affiliate(s) or Ultimate Parent Company in "MUNDRA I TRANSMISSION LIMITED" shall be computed in accordance with the example given below:

If the Parent Company or the Ultimate Parent Company of the Selected Bidder A

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directly holds thirty percent (30%) of the equity in "MUNDRA | TRANSMISSION LIMITED", then holding of Selected Bidder A in "MUNDRA | TRANSMISSION LIMITED" shall be thirty percent (30%);

If Selected Bidder A holds thirty percent (30%) equity of the Affiliate and the Affiliate holds fifty percent (50%) equity in "MUNDRA I TRANSMISSION LIMITED", then, for the purposes of ascertaining the minimum equity/equity lock-in requirements specified above, the effective holding of Bidder A in "MUNDRA I TRANSMISSION LIMITED"shall be fifteen percent (15%), (i.e., 30% x 50%)

- 19.1.5 The provisions as contained in this Article 19.1 shall override the terms of the consortium agreement submitted as part of the Bid.
- 19.1.6 The TSP shall be responsible to report to Nodal Agency, within thirty (30) days from the occurrence of any event that would result in any change in its equity holding structure from that which existed as on the date of signing of the Share Purchase Agreement. In such cases, the Nodal Agency would reserve the right to ascertain the equity holding structure and to call for all such required documents / information / clarifications as may be required.

# 19.2 Commitment of maintaining Qualification Requirement

- 19.2.1 The Selected Bidder will be required to continue to maintain compliance with the Qualification Requirements, as stipulated in RFP Document, till the COD of the Project. Where the Technically Evaluated Entity and/or the Financially Evaluated Entity is not the Bidding Company or a Member in a Bidding Consortium, as the case may be, the Bidding Company or Member shall continue to be an Affiliate of the Technically Evaluated Entity and/or Financially Evaluated Entity till the COD of the Project.
- 19.2.2 Failure to comply with the aforesaid provisions shall be dealt in the same manner as TSP's Event of Default as under Article 13 of this Agreement.

#### 19.3 Language:

- 19.3.1 All agreements, correspondence and communications between the Parties relating to this Agreement and all other documentation to be prepared and supplied under the Agreement shall be written in English, and the Agreement shall be construed and interpreted in accordance with English language.
- 19.3.2 If any of the agreements, correspondence, communications or documents are prepared in any language other than English, the English translation of such agreements, correspondence, communications or documents shall prevail in

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matters of interpretation.

#### 19.4 Affirmation

The TSP and the Nodal Agency, each affirm that:

- a) neither it nor its respective directors, employees, or agents has paid or undertaken to pay or shall in the future pay any unlawful commission, bribe, pay-off or kickback; and
- b) it has not in any other manner paid any sums, whether in Indian currency or foreign currency and whether in India or abroad to the other Party to procure this Agreement, and the TSP and the Nodal Agency hereby undertake not to engage in any similar acts during the Term of Agreement.

# 19.5 Severability

The invalidity or enforceability, for any reason, of any part of this Agreement shall not prejudice or affect the validity or enforceability of the remainder of this Agreement, unless the part held invalid or unenforceable is fundamental to this Agreement.

#### 19.6 Counterparts

This Agreement may be executed in one or more counterparts, each of which shall be deemed an original and all of which collectively shall be deemed one and the same Agreement.

## 19.7 Breach of Obligations/ Roles

The Parties acknowledge that a breach of any of the obligations/ roles contained herein would result in injuries. The Parties further acknowledge that the amount of the liquidated damages or the method of calculating the liquidated damages specified in this Agreement is a genuine and reasonable pre-estimate of the damages that may be suffered by the non-defaulting Party in each case specified under this Agreement.

# 19.8 Restriction of Shareholders / Owners Liability

- 19.8.1 Parties expressly agree and acknowledge that none of the shareholders of the Parties hereto shall be liable to the other Parties for any of the contractual obligations of the concerned Party under this Agreement.
- 19.8.2 Further, the financial liabilities of the shareholder(s) of each Party to this Agreement shall be restricted to the extent provided in the Indian Companies Act, 1956 / Companies Act, 2013 (as the case may be).

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#### 19.9 Taxes and Duties:

- 19.9.1 The TSP shall bear and promptly pay all statutory taxes, duties, levies and cess, assessed/levied on the TSP, its Contractors or their employees that are required to be paid by the TSP as per the Law in relation to the execution of the Project and for providing Transmission Service as per the terms of this Agreement.
- 19.9.2 The Nodal Agency shall be indemnified and held harmless by the TSP against any claims that may be made against the Nodal Agency in relation to the matters set out in Article 19.9.1.
- 19.9.3 The Nodal Agency shall not be liable for any payment of, taxes, duties, levies, cess whatsoever for discharging any obligation of the TSP by the Nodal Agency on behalf of TSP or its personnel, provided the TSP has consented in writing to the Nodal Agency for such work, for which consent shall not be unreasonably withheld.

#### 19.10 No Consequential or Indirect Losses

The liability of the TSP shall be limited to that explicitly provided in this Agreement.

Provided that, notwithstanding anything contained in this Agreement, under no event shall the Nodal Agency or the TSP claim from one another any indirect or consequential losses or damages.

#### 19.11 Discretion:

Except where this Agreement expressly requires a Party to act fairly or reasonably, a Party may exercise any discretion given to it under this Agreement in any way it deems fit.

# 19.12 Confidentiality

- 19.12.1 The Parties undertake to hold in confidence this Agreement and RFP Project Documents and not to disclose the terms and conditions of the transaction contemplated hereby to third parties, except:
  - a) to their professional advisors;
  - to their officers, contractors, employees, agents or representatives, financiers, who need to have access to such information for the proper performance of their activities; or
  - c) disclosures required under Law,

without the prior written consent of the other Parties.

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Provided that, the TSP agrees and acknowledges that the Nodal Agency, may, at any time, disclose the terms and conditions of the Agreement and the RFP Project Documents to any person, to the extent stipulated under the Law and the Competitive Bidding Guidelines.

# 19.13 Order of priority in application:

Save as provided in Article 2.5, in case of inconsistencies between the terms and conditions stipulated in Transmission License issued by the Commission to the TSP, agreement(s) executed between the Parties, applicable Law including rules and regulations framed thereunder, the order of priority as between them shall be the order in which they are placed below:

- terms and conditions of Transmission License;
- applicable Law, rules and regulations framed thereunder;
- this Agreement;
- Agreement(s), if any, under Sharing Regulations.

# 19.14 Independent Entity:

- 19.14.1 The TSP shall be an independent entity performing its obligations pursuant to the Agreement.
- 19.14.2 Subject to the provisions of the Agreement, the TSP shall be solely responsible for the manner in which its obligations under this Agreement are to be performed. All employees and representatives of the TSP or Contractors engaged by the TSP in connection with the performance of the Agreement shall be under the complete control of the TSP and shall not be deemed to be employees, representatives, Contractors of the Nodal Agency and nothing contained in the Agreement or in any agreement or contract awarded by the TSP shall be construed to create any contractual relationship between any such employees, representatives or Contractors and the Nodal Agency.

#### 19.15 Amendments:

19.15.1 This Agreement may only be amended or supplemented by a written agreement between the Parties.

#### 19.16 Waiver:

19.16.1 No waiver by either Party of any default or breach by the other Party in the performance of any of the provisions of this Agreement shall be effective unless in

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writing duly executed by an authorised representative of such Party.

19.16.2 Neither the failure by either Party to insist on any occasion upon the performance of the terms, conditions and provisions of this Agreement nor time or other indulgence granted by one Party to the other Parties shall act as a waiver of such breach or acceptance of any variation or the relinquishment of any such right or any other right under this Agreement, which shall remain in full force and effect.

# 19.17 Relationship of the Parties:

This Agreement shall not be interpreted or construed to create an association, joint venture, or partnership or agency or any such other relationship between the Parties or to impose any partnership obligation or liability upon either Party and neither Party shall have any right, power or authority to enter into any agreement or undertaking for, or act on behalf of, or to act as or be an agent or representative of, or to otherwise bind, the other Party.

## 19.18 Entirety:

- 19.18.1 This Agreement along with its sections, schedules and appendices is intended by the Parties as the final expression of their agreement and is intended also as a complete and exclusive statement of the terms of their agreement.
- 19.18.2 Except as provided in this Agreement, all prior written or oral understandings, offers or other communications of every kind pertaining to this Agreement or the provision of Transmission Service under this Agreement to the Nodal Agency by the TSP shall stand superseded and abrogated.

#### 19.19 Notices:

19.19.1 All notices or other communications which are required to be given under this Agreement shall be in writing and in the English language

19.19.2 If to the TSP, all notices or communications must be delivered personally or by registered post or facsimile or any other mode duly acknowledged to the addressee AESL, Rahul Mathur, rahul-mathur@adoni. Com 13th Floor, South Wing. below:

Address

Attention Email

Fax. No. Telephone No.

KP Epitome - B Block, Makorba, S (n Highway, Ahmedasad - 38005)

M-6359965956

19.19.3 If to the Nodal Agency, all notices or communications must be delivered personally or by registered post or facsimile or any other mode duly acknowledged to the

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addresses below:

#### (i) Central Transmission Utility of India Limited (Nodal Agency)

Address : 5th to 10th Floor, IRCON International Tower,

Tower no-1, Plot no -16, Sector-32, Gurugram,

Haryana:122003

Attention : Ramachandra, Sr GM

Email : ramachand@powergrid.in

Fax. No.

Telephone No. : 9910378128

19.19.4 All notices or communications given by facsimile shall be confirmed by sending a copy of the same via post office in an envelope properly addressed to the appropriate Party for delivery by registered mail. All notices shall be deemed validly delivered upon receipt evidenced by an acknowledgement of the recipient, unless the Party delivering the notice can prove in case of delivery through the registered post that the recipient refused to acknowledge the receipt of the notice despite efforts of the postal authorities.

19.19.5 Any Party may by notice of at least fifteen (15) days to the other Party change the address and/or addresses to which such notices and communications to it are to be delivered or mailed.

#### 19.20 Fraudulent and Corrupt Practices

- 19.20.1 The TSP and its respective officers, employees, agents and advisers shall observe the highest standard of ethics during the subsistence of this Agreement. Notwithstanding anything to the contrary contained in the Agreement, the Nodal Agency may terminate the Agreement without being liable in any manner whatsoever to the TSP, if it determines that the TSP has, directly or indirectly or through an agent, engaged in corrupt practice, fraudulent practice, coercive practice, undesirable practice or restrictive practice in the Bid process. In such an event, the Nodal Agency shall forfeit the Contract Performance Guarantee of the TSP, without prejudice to any other right or remedy that may be available to the Nodal Agency hereunder or subsistence otherwise.
- 19.20.2 Without prejudice to the rights of the Nodal Agency under Clause 19.20.1 hereinabove and the rights and remedies which the Nodal Agency may have under this Agreement, if a TSP is found by the Nodal Agency to have directly or indirectly or through an agent, engaged or indulged in any corrupt practice, fraudulent

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practice, coercive practice, undesirable practice or restrictive practice during the Bid process, or after the issue of Letter of Intent (hereinafter referred to as LoI) or after the execution of the agreement(s) required under Sharing Regulations, the Nodal Agency may terminate the Agreement without being liable in any manner whatsoever to the TSP. Further, the TSP & its Affiliates shall not be eligible to participate in any tender or RFP issued by any BPC for an indefinite period from the date such TSP is found by the Nodal Agency to have directly or indirectly or through an agent, engaged or indulged in any corrupt practice, fraudulent practice, coercive practice, undesirable practice or restrictive practices, as the case may be.

- 19.20.3 For the purposes of this Clause 19.20, the following terms shall have the meaning hereinafter respectively assigned to them:
  - (a) "corrupt practice" means (i) the offering, giving, receiving, or soliciting, directly or indirectly, of anything of value to influence the actions of any person connected with the Bid process (for avoidance of doubt, offering of employment to or employing or engaging in any manner whatsoever, directly or indirectly, any official of the BPC who is or has been associated or dealt in any manner, directly or indirectly with the Bid process or the Lol or has dealt with matters concerning the RFP Project Documents or arising there from, before or after the execution thereof, at any time prior to the expiry of one year from the date such official resigns or retires from or otherwise ceases to be in the service of the BPC, shall be deemed to constitute influencing the actions of a person connected with the Bid Process); or (ii) engaging in any manner whatsoever, whether during the Bid Process or after the issue of the Lol or after the execution of the RFP Project Documents, as the case may be, any person in respect of any matter relating to the Project or the Lol or the RFP Project Documents, who at any time has been or is a legal, financial or technical adviser of the BPC in relation to any matter concerning the Project;
  - (b)"fraudulent practice" means a misrepresentation or omission of facts or suppression of facts or disclosure of incomplete facts, in order to influence the Bid process;
  - (c) "coercive practice" means impairing or harming, or threatening to impair or harm, directly or indirectly, any person or property to influence any person's participation or action in the Bid process;
  - (d) "undesirable practice" means (i) establishing contact with any person connected with or employed or engaged by the BPC with the objective of canvassing, lobbying or in any manner influencing or attempting to influence the Bid process; or (ii) having a Conflict of Interest; and

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(e) "restrictive practice" means forming a cartel or arriving at any understanding or arrangement among Bidders with the objective of restricting or manipulating a full and fair competition in the Bid process;

# 19.21 Compliance with Law:

Despite anything contained in this Agreement but without prejudice to Article 12, if any provision of this Agreement shall be in deviation or inconsistent with or repugnant to the provisions contained in the Electricity Act, 2003, or any rules and regulations made there under, such provision shall be deemed to be amended to the extent required to bring it into compliance with the aforesaid relevant provisions as amended from time to time.



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IN WITNESS WHEREOF, THE PARTIES HAVE CAUSED THIS AGREEMENT TO BE EXECUTED BY THEIR DULY AUTHORISED REPRESENTATIVES AS OF THE DATE AND PLACE SET FORTH ABOVE.

For and on behalf of TSP

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2.

Amit Chatteriee, Manager, AESL [Signature, Name, Designation and Address] 2. For and on behalf of Central Transmission Utility of India Limited (Nodal Agency) [Signature, Name, Designation and Address] WITNESSES: For and on behalf of : BPC (Signature) Amiradolha Khopda H [Insert, Name, Designation and Address of the Witness] For and on behalf of : Nodal Agency (Signature) ROHIT KASGAR, ET CTUIL [Insert Name, Designation and Address of the Witness] Mundra I Transmission Limited Central Transmission Utility of India Limited 70 RANSA NEW DELH

# **SCHEDULES**

Central Transmission Utility of India Limited





# Schedule: 1

#### Project Description and Scope of Project

#### i) Description of the Transmission Scheme:

Ministry of Power has issued Hydrogen Policy vide its letter dated 17-02-2022 with a motive to facilitate the transition from fossil fuel/ fossil fuel-based feedstock to Green hydrogen/ Green ammonia both as energy carriers and chemical feedstock for different sectors. In this respect, MNRE has identified various locations of Green Hydrogen/Ammonia capacities expected to be installed by 2030 along with the electricity demand at these locations. Green Hydrogen/Ammonia manufacturing is planned in the coastal states of Gujarat, Karnataka, Tamil Nadu, Andhra Pradesh, West Bengal and Odisha.

As per MNRE, total electricity demand of Green Hydrogen and Green Ammonia plants/industries in Mundra area of Gujarat will be around 22 GW by 2029-30.

The transmission system for supply of power to upcoming Green Hydrogen and Green Ammonia manufacturing hubs in Western Region was deliberated in Joint Study Meeting amongst CEA, CTU, GRID-INDIA, GETCO, GPCL and TPL held on 23.02.2024 wherein broad transmission system was agreed. The system for evacuation of Green Hydrogen/Ammonia potential in Mundra area of Gujarat was subsequently discussed and agreed in the 26<sup>th</sup> CMETS-WR meeting held on 28.02.2024. Thereafter, the scheme was reviewed in a meeting held 14.08.2024 at CEA wherein the transmission system was finalized to cater to Green Hydrogen/Ammonia potential in Mundra area of Gujarat under Phase-I: Part B1 scheme (3 GW at Navinal S/s) (cumulative upto 4500 MW in Mundra area).

Network Expansion Scheme in Navinal (Mundra) area of Gujarat for drawal of power in the area involves establishment of 4x1500 MVA, 765/400 kV Navinal (Mundra) (GIS) S/s alongwith LILO of Bhuj-II — Lakadia 765 kV D/C line at Navinal (Mundra) (GIS) S/s and is presently under bidding stage. The scheme shall cater to supply of 3000 MW power to Bulk consumers and for meeting 1500 MW demand for Green Hydrogen/Ammonia projects. The subject scheme is for meeting additional 3000 MW drawal requirement of Green Hydrogen/Ammonia projects (cumulative upto 4500 MW in Mundra area) at Navinal (Mundra) (GIS) S/s through Augmentation of Transformation capacity at 765/400 kV Navinal(Mundra) S/s (GIS) by 2x1500 MVA ICTs and Navinal(Mundra) (GIS) — Bhuj 765 kV D/C line.

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# ii) Detailed Scope of Work

Transmission System for supply of power to Green Hydrogen/Ammonia manufacturing potential in Mundra area of Gujarat under Phase-I: Part B1 scheme (3 GW at Navinal S/s)

SI. No.	Scope of the Transmission Scheme	Scheduled COD in months from Effective Date
1.	Augmentation of Transformation capacity at 765/400 kV Navinal(Mundra) S/s (GIS) by 2x1500 MVA ICTs along with 2x330 MVAr, 765 kV and 2x125 MVAr, 420 kV bus reactors on Bus Section-II and 1x125MVAr, 420 kV bus reactor on Bus Section-I. This will involve creation of 765 kV and 400 kV Bus Sections-2 through sectionalization arrangement. The 400 kV and 765 kV Sectionaliser shall be normally closed.  • Creation of New 765 kV and 400 kV Bus Section-II  • 765 kV Sectionaliser – 1 Set  • 400 kV Sectionaliser – 1 Set  • 400 kV Sectionaliser – 1 set  • 765/400 kV, 1500 MVA ICT-2 Nos. (on Sec-II)  • 765 kV ICT bays- 2 Nos. (on Sec-II)  • 400 kV ICT bays- 2 Nos. (on Sec-II)  • 330 MVAr 765 kV bus reactor-2 Nos. (Sec-II)  • 125 MVAr 420 kV bus reactor-3 Nos. (1 No. on Sec-I and 2 Nos. on Sec-II)  • 765 kV reactor bay- 2 Nos. (Sec-II)	36 months from SPV transfer (20.03.2028)

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SI. No.	Scope of the Transmission Scheme	Scheduled COD in months from Effective Date
	400 kV reactor bay- 3 Nos. (1 No. on Sec-I and 2 Nos. on Sec-II)	
2.	Navinal(Mundra) (GIS) — Bhuj 765 kV D/C line	
	765 kV line bays at each end of Navinal(Mundra) (GIS) – Bhuj 765 kV D/C line	
3.	<ul> <li>765 kV line bays-2 Nos. (AIS) (for Bhuj end)</li> <li>765 kV line bays-2 Nos. (GIS) (for Navinal (Mundra) end) (on Sec-II)</li> </ul>	
	±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal(Mundra) (GIS) 400 kV Bus section-I	
. 4.	<ul> <li>±300 MVAr STATCOM along with 2x125MVAr MSC and 1x125MVAr MSR</li> <li>400 kV bay – 1 No.</li> </ul>	
	±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal(Mundra) (GIS) 400 kV Bus section-II	
5.	±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR	
	• 400 kV bay – 1 No.	

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SI. No.	Scope of the Transmission	Scheduled COD in months from
	Scheme	Effective Date

## Note:

- 1) Wherever required, TSP shall implement complete Dia consisting of 2(Two) Main Bays and 1(One) Tie Bay required for completion of diameter (GIS) in one-and-half breaker scheme.
- 2) TSP of Navinal (Mundra) S/s shall provide space for scope of work at Sl. 1, 2, 3 (for Navinal end), 4 and 5 above.
- 3) TSP of Bhuj PS shall provide space for scope of work at Sl. 3 (for Bhuj end) above.

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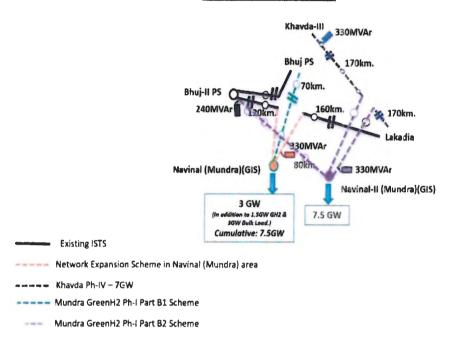




# iii) Transmission Grid Map:

Transmission Grid Map indicating the details of the Project is given below:

## **Transmission Grid Map**



# Location details of existing / proposed substations:

765/400 kV Navinal (Mundra) S/s (GIS): Yet to be finalized by developer.

765 kV Bhuj S/s:23°27'7.44"N, 69°35'37.12"E

**Note:** The above coordinates/location of substation indicated is approximate in the substation area. Exact coordinates for the corresponding bays/gantry for termination of the respective line may be verified and finalized in coordination with actual site.

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# SPECIFIC TECHNICAL REQUIREMENTS FOR TRANSMISSION LINE

- A.1.0 The design, routing and construction of transmission lines shall be in accordance with Chapter V, Part A of CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations 2022, as amended from time to time. Other CEA Regulations/ guidelines as amended up to date and MoP guidelines, as applicable, shall also be followed.
- A.2.0 Selection of tower type shall be made as per CEA Regulations, however, in case lattice type towers are used, the following shall also be applicable:
- A.2.1 Steel section of grade E 250 and/or grade E 350 as per IS 2062, only are permitted for use in towers, extensions, gantry structures and stub setting templates. For towers in snowbound areas, steel sections shall conform to Grade-C of IS-2062.
- A.2.2 The towers shall be designed as per IS-802:2015, however, the drag coefficient of the tower shall be as follows: -

Solidity Ratio	Drag Coefficient
Upto 0.05	3.6
0.1	3.4
0.2	2.9
0.3	2.5
0.4	2.2
0.5 and above	2.0

- A.3.0 The Transmission Service Provider (TSP) shall adopt any additional loading/design criteria for ensuring reliability of the line, if so desired and /or deemed necessary.
- A.4.0 The transmission line shall be designed considering wind zones as specified in wind map given in the National Building Code 2016, Vol.1. The developer shall also make his own assessment of local wind conditions and frequent occurrences of High Intensity Winds (HIW) due to thunderstorms, dust-storms, downburst, etc. along the transmission line route and wherever required, higher wind zone than that given in wind map shall be considered for tower design for ensuring reliability of line. Further, for the transmission line sections passing within a distance of 50 km from the boundary of two wind zones, higher of the two wind zones shall be considered for the design of towers located in such sections.
- A.5.0 Selection of reliability level for design of tower shall be as per CEA Regulation (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations 2022, as amended from time to time.
- A.6.0 A) Under crossing of the existing transmission line of same Voltage shall not be allowed. In the case where it is inevitable to under-cross the existing transmission line then TSP shall seek prior

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approval from Chief Electrical Inspector, CEA with detailed study ensuring that all statutory electrical clearances and Electric Field limit of 10 kV/m at 1 m and 1.8 m from ground level is not violated.

- B) For power line crossing of 400 kV or above voltage level, large angle and dead end towers (i.e. D/DD/QD) shall be used on either side of power line crossing.
- C) For power line crossing of 132 kV and 220 kV (or 230 kV) voltage level, angle towers (B/C/D/DB/DC/DD/ QB/QC/QD) shall be used on either side of power line crossing depending upon the merit of the prevailing site condition and line deviation requirement.
- D) For power line crossing of 66 kV and below voltage level, suspension/tension towers shall be provided on either side of power line crossing depending upon the merit of the prevailing site condition and line deviation requirement.
- E) For crossing of railways, national highways and state highways, the rules/ regulations of appropriate authorities shall be followed.

# A.7.0 The relevant conductor configuration for 765 kV shall be as follows: -

# (i) Navinal (Mundra) (GIS) - Bhuj 765 kV D/C line

Type of conductor: ACSR / AAAC / AL59

**Basic Parameters:** 

Transmission line	ACSR Conductor specified	Equivalent AAAC conductor based on 53% conductivity of Al Alloy	Equivalent minimum size of AL59 conductor based on 59% conductivity of AL Alloy*	Sub- conductor Spacing
765 kV D/C	Zebra :	Stranding details:	Stranding	
(Hexa Bundle)	Stranding	61/3.19 mm,	details:	
transmission	54/3.18 mm-Al +		61/3.08 mm,	
lines	7/3.18 mm-Steel,	487.5 mm <sup>2</sup>		
	428 mm <sup>2</sup>	Aluminium alloy	454 mm <sup>2</sup>	
	Aluminium area,	area	Aluminium alloy	
			area	457 mm
		28.71 mm		
		diameter		

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		27.72 mm
28.62 mm	Maximum DC	diameter
diameter	Resistance at	
	20°C (Ω/km):	Maximum DC
Maximum DC	0.06815	Resistance at
Resistance at		20°C (Ω/km):
20°C (Ω/km):	Minimum UTS:	0.0653
0.06868	135.6 kN	
		Minimum UTS:
Minimum UTS:		108 kN
130.32 kN		

# Note:

- 1. \*To select any size above the minimum, the sizes mentioned in the Indian standard i.e. IS-398(part-6) shall be followed.
- 2. The transmission lines shall have to be designed for a maximum operating conductor temperature of 85° C.
- A.8.0 The required phase to phase spacing and horizontal spacing for 765 kV line shall be governed by the tower design as well as minimum live metal clearances for 765 kV voltage level under different insulator swing angles. However, the phase to phase spacing for 765 kV line shall not be less than 15 m.
- A.9.0 All electrical clearances including minimum live metal clearance, ground clearance and minimum mid span separation between earth wire and conductor as given below shall be considered:

# Minimum live metal clearances for 765 kV line:

a) (i) Under stationary conditions

From tower body: For 765 kV D/C: 6.1 m

For 765 kV S/C: 5.6 m

(ii) Under swing conditions

	Wind Pressure Condition	Minimum Electrical Clearance
a)	Swing angle (25º)	4.4 m
b)	Swing angle (55º)	1.3 m

b) Minimum ground clearance for 765 kV line: 18 m

c) Minimum mid span separation between earth-wire and conductor for 765 kV line: 9.0 m

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- A.10.0 The shielding angle shall not exceed 10 deg for 765 kV D/C transmission line.
- A.11.0 The Fault current for design of line shall be 50 kA for 1 sec for 765 kV.
- A.12.0 In case of 400 kV and above voltage class lines, at least one out of two earth wires shall be OPGW and second earth wire, if not OPGW, shall be either of Galvanized Standard Steel (GSS) or Aluminum Alloy Conductor Steel Reinforced (AACSR) or any other suitable conductor type depending upon span length and other technical consideration.
- A.13.0 Each tower shall be earthed such that the tower footing impedance does not exceed 10 ohms (Ω). Pipe type or Counterpoise type earthing shall be provided in accordance with relevant IS. Additional earthing shall be provided on every 7 to 8 km distance for direct earthing of both shield wires. If site condition demands, multiple earthing or use of earthing enhancement compound shall be used.
- A.14.0 Pile type foundation shall be used for towers located in river or creek bed or on bank of river having scourable strata or in areas where river flow or change in river course is anticipated, based on detailed soil investigation and previous years' maximum flood discharge of the river, maximum velocity of water, highest flood level, scour depth and anticipated change in course of river based on river morphology data of at least past 20 years to ensure availability and reliability of the transmission line.
- A.15.0 Transmission line route shall be finalized, in consultation with appropriate authorities so as to avoid the habitant zones of endangered species and other protected species. Bird diverters, wherever required, shall be provided on the transmission line. In order to optimize the route, use of GATISHAKTI platform shall also be made.
- A.16.0 Wherever, the transmission lines are passing through cyclone prone areas i.e. areas upto 60 km from coast following shall also be applicable:
  - a) Terrain category-I, with terrain roughness factor (K2) of 1.08 shall be considered for tower design for exposed open terrain with few or no obstruction which also includes open sea coasts, open stretch of water, desert and flat treeless plains
  - b) Importance factor for cyclonic region (K4) of 1.3 shall be considered for tower design.
  - c) The number of consecutive spans between the section points/ angle point shall not exceed 10 spans or 3km instead of conventional practice of 15 spans or 5km, in order to reduce the failure of such towers in coastal areas due to cascading effect. The section shall be terminated with tension tower/ angle tower and angle of deviation should be based on the site requirement.
- A.17.0 Wherever, the transmission lines are passing through cyclone prone areas (i.e. areas upto 60 km from coast)/ creek regions/ aggressive soil areas following shall also be applicable:

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- a) The fabricated tower parts and stubs shall have a minimum overall zinc coating of 900 g/m<sup>2</sup> of surface area except for plates and sections below 5 mm which shall have a minimum overall zinc coating of 610 g/m<sup>2</sup> of surface area. The average zinc coating for all sections and plates 5 mm and above shall be maintained as 127 micron and that for plates and sections below 5 mm shall be maintained as 87 micron.
- b) Ready mix concrete of M30 Grade shall be used to avoid use of locally available saline water. However, the design mix concrete of M30 Grade conforming to IS 456 with potable water can be used at locations where transportation of ready-mix concrete is not feasible. The minimum cement content in any case shall not be less than 330 kg/m<sup>3</sup>.
- c) The surface of the reinforced steel shall be treated with epoxy-based coating to enhance corrosion performance of the foundations. Use of epoxy coated reinforcement in foundation shall be as per IS 13620. In addition, two (2) coats of bituminous painting of minimum 1.6 kg/m² per coat shall be applied on all exposed faces of foundation (i.e. pedestal and base slab).
- d) Double coat 20 mm thick cement plaster shall be provided on all exposed concrete surface as well up to 300 mm below ground level to give protection to concrete surface from environmental and saline effect.
- e) Before coping of chimney top portion, three coats of anti-corrosive paint of minimum 30-35 micron dry film thickness each shall be applied on the stub in the 50 mm coping portion as well as up to 350 mm above CL portion.
- A.18.0 The raised chimney foundation is to be provided in areas prone to flooding/water stagnation like paddy field/agricultural field and undulated areas to avoid direct contact of water with steel part of tower. The top of the chimney of foundation should be at least above High Flood Level (HFL) or the historical water stagnation/ logging level (based on locally available data) or above High Tide Level or 500 mm above Natural Ground Level (whichever is higher).
- A.19.0 Routing of transmission line through protected areas of India shall be avoided to the extent possible. In case, it is not possible to avoid protected areas, the towers of the transmission line up to 400 kV level which are installed in protected areas shall be designed for Multi-circuit (4 circuits) configuration of same voltage level considering reliability level of at least two (2). The top two circuits of these multi-circuit towers shall be used for stringing of the transmission line under present scope and the bottom two circuits shall be made available for stringing of any future transmission line of any transmission service providers/ State transmission utilities/Central transmission utilities passing through the same protected area. Further, the configuration and coordinates of such transmission towers shall be submitted to CEA, CTU and BPC by the TSP.

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- A.20.0 The TSP shall abide by the Guidelines of CEA w.r.t. shifting of transmission lines for NHAI projects and other projects.
- A.21.0 The safety precautions in regards to gas/oil pipe lines in vicinity of Transmission lines shall be taken in coordination with gas/ petroleum authorities.
- A.22.0 The stringing of the transmission line in forest area shall be carried out through drone.
- A.23.0 RoW width and Span in different terrain shall be as per Schedule VII of CEA (Technical Standards for Construction of Electrical plants and Electric Lines) Regulations 2022 and RoW guidelines issued vide CEA-PS-14-86/2/2019-PSETD Division dated 24.09.2024

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#### SPECIFIC TECHNICAL REQUIREMENTS FOR SUBSTATION

Extension of 765/400 kV Navinal (Mundra) S/s shall be Gas Insulated Switchgear (GIS) type conforming to the requirements of CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations 2022, as amended from time to time.

The extension of 765/400/220 kV **Bhuj S/s** shall be conventional Air Insulated Switchgear (AIS) type conforming to the requirements of CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations, 2022, as amended from time to time.

Other CEA Regulations/guidelines as amended up to date and MoP guidelines, as applicable, shall also be followed.

# **B.1.0** Salient features of Substation Equipment and Facilities

The design and specification of substation equipment are to be governed by the following factors:

#### **B.1.1** Insulation Coordination

The system design parameters for substations/switchyards shall be as given below:

SI. No.	Description of parameters	765/400 kV Navinal (Mundra) (GIS) Extn.		765 kV Bhuj PS (AIS) Extn.	
		765 kV System	400 kV System	765 kV System	
1.	System operating voltage	765 kV	400 kV	765 kV	
2.	Maximum voltage of the system (rms)	800 kV	420 kV	800 kV	
3.	Rated frequency	50 Hz	50 Hz	50 Hz	
4.	No. of phases	3	3	3	
5.	Rated Insulation Levels			11-11-11-11-11-11-11-11-11-11-11-11-11-	
i)	Lightning Impulse Withstand Voltage for (1.2/50 micro sec.) - for Equipment other than Transformer and reactor	2100 kVp	1425 kVp	2100 kVp	
	- for Insulator String	2100 kVp	1550 kVp	2100 kVp	
ii)	Switching Impulse Withstand Voltage (250/2500 micro sec.) dry and wet	1425 kVp	1050 kVp	1550 kVp	

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SI. No.	Description of parameters	765/400 kV Navinal (Mundra) (GIS) Extn.		765 kV Bhuj PS (AIS) Extn.	
		765 kV	400 kV	765 kV	
		System	System	System	
iii)	One minute power frequency dry	gegegenergenergy om det delst, signis symmetic medical branch om siglisteritority och sill det delst	A CONTRACTOR OF THE CONTRACTOR		
	withstand voltage (rms)	960 kV	650 kV	830 kV	
6.	Corona Extinction Voltage	508 kV	320 kV	508 kV	
7.	Max. radio interference voltage for	2500 micro-	1000 micro-	2500 micro-volts	
	frequency between 0.5 MHz and 2	volt at 508 kV	volt at 266	at 508 kV rms	
	MHz	rms	kV rms		
8.	Minimum creepage distance for	24800 mm	13020 mm	24800 mm	
	insulator string/longrodinsulators/outdoorbushings	(31 mm/kV)	(31 mm/kV)	(31 mm/kV)	
9.	Minimum creepage distance for	24800 mm	13020 mm	24800 mm	
	switchyardequipment	(31 mm/ kV)	(31 mm/ kV)	(31 mm/ kV)	
10.	Max. Fault Current	50 kA	63 kA	50 kA	
11.	Duration of Fault	1 sec	1 sec	1 sec	

# **B.1.2** Switching Scheme

The switching schemes, as mentioned below, shall be adopted at various voltage levels of substation/switchyard:

Substation	765 kV side	400 kV side	
Extension of 765/400 kV Navinal (Mundra) (GIS)	One and Half Breaker	One and Half Breaker	
Extension of 765 kV Bhuj PS (AIS)	One and Half Breaker	N/A	

# Notes: -

- i) For one and half breaker switching scheme, any double circuit line consisting of two numbers of feeders and originating from the same transmission or generating switchyard shall not be terminated in one diameter.
- ii) Two transformers of the same HV rating shall not be connected in the same diameter and similarly two bus reactors of same HV rating shall also not be connected in the same diameter.
- iii) A diameter in one and half breaker scheme is a set of 3 circuit breakers with associated isolators, earth switches, current transformers etc. for controlling 2 numbers of feeders.
- iv) In case of GIS substation where the bus scheme is One and Half breaker scheme, the

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- diameters shall be complete with feeder/line side isolator and GIS duct of the future bay shall be brought outside the GIS hall/building with extension/interface module suitably.
- v) Connection arrangement of Switchable Line reactors shall be such that it can be used as Line reactor as well as Bus reactor with suitable NGR bypass arrangement. Further, Spare 1-phase Shunt Reactor unit shall be placed and connected in such a way that the spare unit can be utilized for all the bus and switchable line reactor banks (including future reactor banks) without its physical movement.
- vi) Provision of Bus sectionalizer:
  - One (1) set of bus sectionalizer for 765 kV shall comprise 2 Nos. of bus sectionalizer bays with associated Circuit Breakers, Isolators and Current Transformers for both buses.

    One (1) set of bus sectionalizer for 400 kV shall comprise 2 Nos. of bus sectionalizer bays with
- vii) TSP shall plan distribution of line and transformer feeders to bus bar in such a way that all power can be evacuated successfully without crossing thermal limit at any point of bus-bar.

associated Circuit Breakers, Isolators and Current Transformers for both buses.

# viii) 765/400 kV Navinal (Mundra):

765 kV bay configurations (one and half breaker scheme) shall be as follows:

Configuration	Numbers
ICT- Tie- Line	1 (one,
Bus Reactor- Tie- Line	1 (one,
ICT- Tie- Bus Reactor	1 (one,

400 kV bay configurations (one and half breaker scheme) shall be as follows:

Configuration	Numbers
400 kV Bus Section-I	
Bus Reactor-Tie-STATCOM	1 (one)
400 kV Bus Section-II	
ICT (400 kV side of 765 kV ICT)- Tie- Future Line with Switchable Line Reactor*	1 (one)
ICT (400 kV side of 765 kV ICT)- Tie- Bus Reactor	1 (one)
STATCOM- Tie- Bus Reactor	1 (one)

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Note (\*): GIS modules for future Line bay and Switchable Line Reactor bay shall be provided by TSP under present scope and GIS duct shall be brought outside the GIS half/building with extension/interface module suitably.

ix) 765 kV Bus Sectionalization shall be with the following feeder distribution.

765kV Bus Section-1 (Existing)	765kV Bus Section-2 (Present)		
a) 4 Nos. of existing 765 kV Line	a) 2 Nos. of present 765 kV line		
b) 4 Nos. of existing 765/400 kV IC	T b) 2 Nos. of present 765/400 kV ICT		
c) 2 Nos. of existing 765 kV Bus	c) 2 Nos. of present 765 kV Bus		
Reactor	Reactor		
	d) 3 Nos. of future 765/400 kV ICT		
	e) 4 Nos. of future 765 kV line along		
	with switchable line reactor		

x) 400kV Bus Sectionalization shall be with the following feeder distribution.

	400kV Bus Section-1 (Existing)	400kV Bus Section-2 (Present)		
a)	4 Nos. of existing 765/400 kV ICT	a) 2 Nos. of present 765/400 kV ICT		
b)	1 No. of existing Bus Reactor	b) 2 Nos. of present 400 kV Bus Reactor		
c)	MUL-Navinal (Mundra) (GIS)	c) 1 No. STATCOM (Present)		
	2xD/C (existing)	d) 3 Nos. of future 765/400 kV ICT		
d)	2 Nos. of future 400 kV Line	e) 3 Nos. of future 400/220 kV ICT		
	alongwith switchable line reactor	f) 8 Nos. of future 400 kV Line along		
e)	3 Nos. of future 400/220 kV ICT	with switchable line reactor		
f)	1 No. of present 400 kV Bus			
	Reactor			
g)	1 No. of present STATCOM			

- xi) 765 kV Bhuj Extn: One circuit of Navinal (Mundra (GIS)) Bhuj 765 kV D/C line shall be terminated in bay no. 716 (associated tie bay is already existing) and other circuit shall be terminated in bay no. 713 (associated tie bay is already existing) as per SLD provided with the RfP.
- xii) Further, all associated interconnection work shall also be in the present scope of TSP.

# **B.2.0** Substation Equipment and facilities (Voltage level as applicable):

The switchgear shall be designed and specified to withstand operating conditions and duty requirements. All equipment shall be designed considering the following capacity.

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SI. No	No Description of bay	Extn of 765/400 kV Navinal (Mundra) (GIS)		Extn of 765 kV Bhuj PS
		765 kV	400 kV	765 kV
1.	Bus Bar	4000A	4000A	As per existing
2.	Line bay	3150 A	3150 A	3150 A
3.	ICT bay	3150 A	3150 A	N/A
4.	Reactor bay	3150 A	3150 A	N/A
5.	STATCOM Bay	N/A	3150 A	N/A

#### **B.2.1** Power Transformers

# B.2.1.1 $(765/\sqrt{3})/(400/\sqrt{3})/33$ kV Single Phase Autotransformer

500 MVA 765/ $\sqrt{3}$ )/(400/ $\sqrt{3}$ )/33 kV, 1-phase Autotransformer (including arrangement for 3-phase bank formation of 1500 MVA) shall conform to CEA's "Standard Specifications and Technical Parameters for Transformers and Reactors (66 kV and above voltage class)" as amended up to date available on CEA website.

Connection arrangement for utilization of existing Spare Single Phase Autotransformer unit: TSP shall make the arrangement of present ICT bank in such a way that the existing spare unit can be utilized for Transformer bank under present scope without its physical movement.

# **B.2.2** Shunt Reactors

# B.2.2.1 (765/ $\sqrt{3}$ ) kV Single Phase Shunt Reactor

110 MVAr, 765/ $\sqrt{3}$  kV, 1-Phase Reactor (including arrangement for 3-phase bank formation of 330 MVAr) shall conform to CEA's "Standard Specifications and Technical Parameters for Transformers and Reactors (66 kV and above voltage class)" as amended up to date available on CEA website.

Connection arrangement for utilization of existing Spare Single Phase Reactor unit: TSP shall make the arrangement of present reactor bank in such a way that the existing spare unit can be utilized for reactor bank under present scope without its physical movement.

# B.2.2.2 420 kV, 3-Phase, Shunt Reactor

125 MVAr, 420 kV, 3-Phase Reactor shall conform to CEA's "Standard Specifications and Technical Parameters for Transformers and Reactors (66 kV and above voltage class)" as amended up to date available on CEA website.

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# B.2.3 765 kV and 400 kV GiS Substation equipment

GIS (Gas Insulated Switchgear) shall be Indoor type in accordance to IEC: 62271-203. The switchgear shall be designed and specified to withstand operating conditions and duty requirements. All the switchgear such as Circuit Breaker, isolator, earth switch including CT, PT etc. shall be GIS type. The Surge Arrestor and Voltage Transformer shall be either GIS or outdoor AIS type.

The GIS assembly shall consist of separate modular compartments e.g. Circuit Breaker compartment, Bus bar compartment filled with SF<sub>6</sub> Gas and separated by gas tight partitions so as to minimize risk to human life, allow ease of maintenance and limit the effects of gas leaks failures and internal arcs etc. These compartments shall be designed to minimize the risk of damage to adjacent sections and protection of personnel in the event of a failure occurring within the compartments. Rupture diaphragms with suitable deflectors shall be provided to prevent uncontrolled bursting pressures developing within the enclosures under worst operating conditions, thus providing controlled pressure relief in the affected compartment. The arrangement of gas sections or compartments shall be such as to facilitate future extension of any make without any drilling, cutting or welding on the existing equipment. To add equipment, it shall not be necessary to move or dislocate the existing switchgear bays. The layout of Gas Insulated Bus Ducts shall be properly planned to optimize the length of bus ducts and for easy accessibility for maintenance. The length of bus bars, bus ducts, isolator sections shall be optimized considering effects of fast transient voltage due to isolator operations.

The bus bar modules including auxiliary bus modules (wherever applicable) shall be provided with suitable End Piece (Interface) module with the test link facility for future extension as per provisions of future requirements. The end piece module shall be designed in such a way so that future GIS modules may be tested without extending test voltage to existing bus and vice-versa by removing the test link.

TSP shall make available the complete details for the design of interface module such as cross section, enclosure material, enclosure dimensions (inner and outer), Flange diameter (inner and outer), conductor cross-section and connection arrangement, bolt spacing and dimension, rated gas pressure, Gasket detail etc. Further, adequate space for GIS bus bar interface module shall be taken into account for future scope.

Each section shall have plug-in or easily removable connection pieces to allow for easy replacement of any component with the minimum disturbance to the remainder of the equipment. Inspection windows (View Ports) shall be provided for Disconnector Switches and both type of earth switches i.e. Maintenance and fast operating.

Local Control Cabinets (LCC) shall be provided as per requirement. The alarm and annunciation of GIS equipment shall be wired to the Supervisory Control and Data Acquisition (SCADA) System.

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The material and thickness of the enclosures shall be such as to withstand an internal flashover without burns through for a period of 300 ms at rated short time withstand current. The material shall be such that it has no effect of environment as well as from the by-products of SF<sub>6</sub> breakdown under arcing conditions. This shall be validated with Type Test.

## Service continuity requirement for GIS:

The GIS equipment with the given bus switching arrangement shall be divided into different gas compartments. During the work such as a fault repair or major maintenance, requiring the dismantling of a gas compartment for which more than one compartments may need to be degassed.

TSP shall meet following Service continuity conditions (to the extent possible) with ensuring equipment and operating personnel's safety:

- For One and Half breaker bus switching scheme, during a fault in Circuit Breaker compartment, no bus bar and feeder is permitted out of service during maintenance and repair/replacement.
- During a fault in a GIS compartment other than the Circuit Breaker compartment, maximum
  of one bus bar and/or one feeder is permitted out of service during maintenance and
  repair/replacement.

## UHF sensors in GIS for PD (Partial Discharge) detection:

The adequate number of Ultra High Frequency (UHF) sensors shall be provided in the offered GIS alongwith suitable portable type Partial Discharge (PD) measuring instrument for detection of Partial discharge (of 5 pC and above as per IEC 60270). The number and location of these sensors shall be based on laboratory tests on the typical design of GIS as per recommendations of CIGRE Document No. 654 (Application Guide for sensitivity verification for UHF Partial discharge detection system for GIS).

# B.2.3.1 Circuit Breakers (GIS)

GIS Circuit breakers shall in general be of C2-M2 class and comply to IEC-62271-100. The rated break time shall not exceed 40 ms (milli second) for 765 kV and 400 kV. Circuit breakers shall be suitable for single phase and three phase auto reclosing. Each breaker would have two sets of trip circuits which would be connected to separate DC supplies for greater reliability. The Circuit breakers controlling 765 kV lines shall be provided with pre-insertion closing resistor of about 450 ohms with 9 ms insertion time or Controlled Switching Device (CSD). The Circuit breakers controlling 400 kV lines wherever required shall be provided with pre-insertion closing resistor of about 400 ohms with 8 ms insertion time or Controlled Switching Device (CSD) for lines longer than 200 km. The short line fault capacity shall be the same as the rated capacity and this is proposed to be achieved without use of opening resistors. Controlled switching device shall be

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provided in the Circuit Breaker of the switchable line reactor bay and in Main and Tie bay circuit breakers of line with non-switchable line reactors, Bus reactors and Transformers for 400 kV and above voltage class.

## B.2.3.2 Isolators (GIS)

The isolators shall comply to IEC 62271-102 in general. Earth switches shall be provided at various locations to facilitate maintenance. Main blades and earth blades shall be interlocked and interlock shall be fail safe type. All isolators and earth switches shall be motor operated type.

The isolator shall be of extended mechanical endurance class-M2 and suitable for Bus Transfer Current Switching duty as per IEC standards. High speed earthing switches shall be provided for grounding purposes at overhead line terminations and cable terminations and shall have fault making capability as specified. Earth switch for line isolator shall be of earthing switch class E1 and shall be suitable for induced current switching duty as defined for Class-B as per relevant standard.

# **B.2.3.3** Current Transformers (GIS)

Current Transformers shall comply with IEC 61869 in general. All ratios shall be obtained by secondary taps only. Generally, Current Transformers (CT) shall have five cores (four for protection and one for metering) whereas; CT in Tie bays shall have six cores (four for protections and two for metering) suitably distributed on both sides of CB (for 400 kV and above voltage class). The burden and knee point voltage shall be in accordance with the requirements of the system including possible feeds for telemetry. The accuracy class for protection core shall be PX and for the metering core it shall be 0.25. The rated burden of cores shall be closer to the maximum burden requirement of metering and protection system (not more than 20 VA for metering core) for better sensitivity and accuracy.

The instrument security factor shall be less than 5 for CTs upto 400 kV voltage class and less than 10 for CTs of 765 kV voltage class.

## B.2.3.4 Voltage Transformer (GIS)

The voltage transformers shall conform to IEC-61869. Voltage transformers shall be of electromagnetic type with SF<sub>6</sub> gas insulation. The earth end of the high voltage winding and the ends of the secondary winding shall be brought out in the terminal box. The voltage transformers shall be located as a separate bay module and will be connected phase to ground and shall be used for protection, metering and synchronization. The voltage transformers shall be of inductive type, nonresistant and shall be contained in their own-SF6 compartment, separated from other parts of installation. The voltage transformer shall be effectively shielded against high frequency electromagnetic transients. The voltage transformer shall have three secondary windings out of

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which two shall be used for protection and one for metering. The voltage transformer should be thermally and dielectrically safe when the secondary terminals are loaded with the guaranteed thermal burdens. The accuracy class for protection cores shall be 3P. The accuracy of 0.2 on metering core should be maintained throughout the entire burden range on all the three windings without any adjustments during operation. The rated burden of cores shall be closer to the maximum burden requirement of metering and protection system (not more than 50 VA for metering core) for better sensitivity and accuracy.

## B.2.3.5 Surge Arresters (GIS) (if applicable)

624 kV Station High (SH) duty and 336 kV Station High (SH) duty gapless type Surge arresters with thermal energy (Wth) of minimum 13 kJ/kV and 12 kJ/kV respectively shall be provided for 800 kV and 420 kV system respectively conforming to IEC 60099-4 in general. Other characteristics of Surge arrester shall be chosen in accordance with system requirements. Surge arresters shall be provided at line entrances, near transformers and reactors so as to achieve proper insulation coordination. A leakage current monitor with surge counter shall be provided with each surge arrester.

## B.2.3.6 SF<sub>6</sub> to Air Bushing

Outdoor bushings, for the connection of conventional external conductors to the SF<sub>6</sub> metal enclosed switchgear, shall be provided. Bushings shall generally be in accordance with the requirements of IEC-60137. The creepage distance over the external surface of outdoor bushings shall not be less than 31 mm/kV. SF<sub>6</sub> to air Bushing shall be of Polymer/ composite type and shall be robust and designed for adequate cantilever strength to meet the requirement of seismic conditions. The electrical and mechanical characteristics of bushings shall be in accordance with IEC-60137. Polymer/composite insulator shall be seamless sheath of silicon rubber compound. The housing and weather sheds should have silicon content of minimum 30% by weight. It should protect the bushing against environmental influences, external pollution and humidity. The hollow silicon composite insulators shall comply with the requirements of IEC 61462 and the relevant parts of IEC-62217.

# B.2.4 765 kV and 400 kV AIS Substation equipment (as applicable)

# **B.2.4.1** Circuit Breakers (AIS)

The circuit breakers and accessories shall conform to IEC: 62271-100, IEC: 62271-1 and shall be of SF<sub>6</sub> Type. The circuit breakers shall be of class C2-M2 (as per IEC) with regard to restrike probability during capacitive current breaking and mechanical endurance. The rated break time shall not exceed 40 ms for 765 kV circuit breakers. The 765 kV circuit breakers shall be provided with single phase and three phase auto reclosing. Each breaker would have two sets

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of trip circuits, which would be connected to separate DC supplies for greater reliability. The circuit breakers controlling 765 kV lines shall be provided with pre-insertion closing resistor of about 450 ohm maximum with 9 ms insertion time or Controlled Switching Device. The short line fault capacity shall be same as the rated capacity and this is proposed to achieve without use of opening resistors. The controlled switching device shall be provided in circuit breakers of switchable line reactor bay and in Main and Tie bay circuit breakers of line with non-switchable line reactors, Bus Reactors and Transformers of voltage class 400 kV and above.

# B.2.4.2 Isolators (AIS)

The isolators shall comply with IEC 62271-102 in general. 765 kV Isolator design shall be double break or vertical break or knee-type. All isolators and earth switches shall be motor operated. Earth switches shall be provided at various locations to facilitate maintenance. Isolator shall be of extended mechanical endurance class – M2 as per IEC-62271-102. Main blades and earth blades shall be interlocked and interlock shall be fail safe type. The 765 kV earth switch for line isolator shall be suitable for induced current switching duty as defined for Class-B.

#### **B.2.4.3** Current Transformers (AIS)

Current Transformers shall comply with IEC 61869 in general. All ratios shall be obtained by secondary taps only. Generally, Current Transformers (CT) for 765 kV shall have six cores (four for protection and two for metering). The burden and knee point voltage shall be in accordance with the requirements of the system including possible feeds for telemetry. The accuracy class for the protection core shall be PX and for the metering core it shall be 0.25. The rated burden of cores shall be closer to the maximum burden requirement of the metering and protection system (not more than 20 VA for metering core) for better sensitivity and accuracy. The instrument security factor shall be less than ten (10) for CTs of 765 kV voltage class.

## **B.2.4.4** Capacitive Voltage Transformers (AIS)

Capacitive Voltage transformers shall comply with IEC 61869 in general. These shall have three secondaries out of which two shall be used for protection and one for metering. Accuracy class for protection cores shall be 3P and for metering core it shall be 0.2. The Capacitive voltage transformers on lines shall be suitable for Carrier Coupling. The Capacitance of CVT for 765 kV shall be 8800 pF. The rated burden of cores shall be closer to the maximum burden requirement of metering and protection system (not more than 50 VA for metering core) for better sensitivity and accuracy.

#### **B.2.4.5** Surge Arresters (AIS)

624 kV Station High (SH) duty and 336 kV Station High (SH) duty gapless type Surge arresters with thermal energy (Wth) of minimum 13 kJ/kV and 12 kJ/kV respectively shall be provided for 800

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kV and 420 kV system respectively conforming to IEC 60099-4 in general. Other characteristics of Surge arrester shall be chosen in accordance with system requirements. Surge arresters shall be provided at line entrances, near Transformers and Reactors so as to achieve proper insulation coordination. Surge Arresters shall be provided with porcelain/ polymer housing fitted with pressure relief devices. A leakage current monitor with surge counter shall be provided with each surge arrester.

## **B.2.5** Protection Relaying and Control System

The protective relaying system proposed to be provided for transmission lines, autotransformers, reactors and bus bars to minimize the damage to the equipment in the events of faults and abnormal conditions, is dealt in this section. All main protective relays shall be numerical type with IEC 61850 communication interface and should have interoperability during integration of numerical relays to communicate over IEC61850 protocol with RTU/SAS/IEDs of different OEMs. All numerical relays shall have built in disturbance recording feature.

The protection circuits and relays of transformer and reactor shall be electrically and physically segregated into two groups each being independent and capable of providing uninterrupted protection even in the event of one of the protection groups failing, to obtain redundancy, and to take protection systems out for maintenance while the equipment remains in service.

## a) Transmission Lines Protection

765 kV and 400 kV (voltage level as applicable) lines shall have Main-I numerical three zone distance protection scheme with carrier aided inter-tripping feature. 765 kV and 400 kV lines shall also have Main-II numerical distance protection scheme like Main-I but from different make that of Main-I. The Main-I and Main-II protection relays of same make may be provided only if they are of different hardware and manufacturing platform or different principle of operation.

However, Line Current Differential relay (with back up distance protection feature) as Main–I and Main-II shall be considered at both ends for short lines (line length below 30 km) having Fibre Optic communication link. Differential relay at remote end shall be provided by the TSP. Associated power and control cabling and integration with SAS at remote end shall be provided by respective bay owner.

In case of loop in loop out of transmission lines, the existing protection scheme shall be studied and suitable up-gradation (if required) shall be carried out.

Further, all 765 kV and 400 kV lines shall be provided with single and three phase auto-reclosing facility to allow reclosing of circuit breakers in case of transient faults. These lines shall also be provided with distance to fault locators to identify the location of fault on transmission lines.

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All 765 kV and 400 kV lines shall also be provided with two stages over voltage protection. Over voltage protection and distance to fault locator may be provided as in-built feature of Main-I and Main-II protection relays. Auto reclose as built-in function of Bay Control Unit (BCU) is also acceptable.

The Main-I and Main-II protection relays shall be fed from separate DC sources and shall be mounted in separate panels.

For 765 kV and 400 kV transmission lines, directional IDMT earth fault relay should be provided as standalone unit or in-built feature of Main-I and Main -II feature.

# b) Autotransformer Protection

These shall have the following protections:

- (i) Numerical Differential Protection
- (ii) Numerical Restricted Earth Fault Protection
- (iii) Numerical Back-up Over-current and Earth Fault Protection on High Voltage (HV) and Intermediate Voltage (IV) side
- (iv) Numerical Over Fluxing Protection on HV and IV side
- (v) Numerical Overload Alarm

Further, Numerical Back-up Over-current and earth fault protection on HV and IV side of autotransformer shall not be combined with other protective functions in the main relays and shall be independent relays. Besides these, power transformers shall also be provided with Buchholz relay, Magnetic Oil Gauge (MOG) with low oil level alarm, protection against high oil and winding temperature and pressure relief device etc.

Suitable monitoring, control (operation of associated circuit breaker and isolator) and protection for LT auxiliary transformer connected to tertiary winding of auto-transformer for the purpose of auxiliary supply shall be provided. The over current and other necessary protection shall be provided for the auxiliary transformer. These protection and control may be provided as built in feature either in the bay controller to be provided for the auxiliary system or in the control and protection IEDs to be provided for autotransformer.

#### c) 765 kV and 400 kV Reactor Protection

Reactor shall be provided with the following protections:

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- i) Numerical Differential protection.
- ii) Numerical Restricted Earth Fault protection
- iii) Numerical Back-up Impedance protection

Besides these, reactors shall also be provided with Buchholz relay, Magnetic Oil Gauge (MOG) with low oil level alarm, protection against oil and winding temperatures and pressure relief device, etc.

## d) Busbar Protection

The high speed low impedance type bus bar differential protection, which is essential to minimize the damage and maintain system stability at the time of bus bar faults, shall be provided for 765 kV and 400 kV. Duplicated bus bar protection is envisaged for 765 kV and 400 kV bus-bar protection. Bus bar protection scheme shall be such that it operates selectively for each bus and incorporate necessary features required for ensuring security.

Bus Bar protection system for new substation shall be de-centralized (distributed) type.

The scheme shall have complete bus bar protection for present as well as envisaged future bays i.e. input / output modules for future bays for the bus sections under present scope and PUs shall be provided by the respective bay owners.

In case, the bus section is provided, then each side of bus section shall have separate set of bus bar protection schemes.

For existing substations, the existing bus bar protection shall be augmented as per requirement.

#### e) Local Breaker Back up Protection

This shall be provided for each 765 kV and 400 kV circuit breakers and will be connected to deenergize the affected stuck breaker from both sides.

#### Notes:

- 1. LBB and REF relays shall be provided separately from transformer differential relay.
- LBB relay may also be provided as built-in protection function of distributed bus bar protection scheme; however in such case separate LBB relay shall be provided for tie bays (in case of One and Half breaker scheme).
- 3. Over fluxing and overload protection can be provided as built-in feature of differential relay.
- 4. In 765 kV and 400 kV switchyard, if spare bay of half diameter is identified as future, Tie CB relay panel shall be with Auto-reclosure feature.
- The bay(s) executed for future utilization under diameter completion, circuit breaker protection panel(s) shall be provided under present scope.

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#### B.2.6 Substation Automation System

For all the new substations, state of art Substation Automation System (SAS) conforming to IECa) 61850 shall be provided. The distributed architecture shall be used for Substation Automation system, where the controls shall be provided through Bay control units. The Bay Control Unit (BCU) is to be provided bay wise for voltage level 220 kV and above. All Bay Control Units (BCU) as well as protection units are normally connected through an Optical fibre high speed network. The control and monitoring of circuit breaker, dis-connector, re-setting of relays etc. can be done from Human Machine Interface (HMI) from the Relay Control Room.

The functions of control, annunciation, disturbance recording, event logging and measurement of electrical parameters shall be integrated in Substation Automation System (SAS).

At new substations, the Substation Automation System (SAS) shall be suitable for operation and monitoring of the complete substation including proposed future bays/elements.

In existing substations with Substation automation system (SAS), augmentation of existing SAS shall be done for bays under present scope.

In existing Substations where Substation automation is not provided, control functions shall be done through control panels.

Necessary gateway and modems (as required) shall be provided to send data to RLDC/SLDC as per their requirement and shall be provisioned with 2+2 redundancy i.e. 2 channels for Main Control Centre and 2 channels for Backup Control Centre. In order to meet this requirement, suitable redundancy at port and card level need to be ensured by the TSP to avoid any single point of failure which may lead to interruption in real-time grid operation. Accordingly, all the hardware for communication services of station as stated above shall support dual redundancy for data transmission of station to respective main and backup RLDCs. Any augmentation work at RLDC/SLDC is excluded from TSP's scope. However, all the configuration work at substation end required to send data to RLDC/SLDC shall be in the scope of TSP.

#### **Time Synchronization Equipment** b)

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Time Synchronization Equipment complete in all respect including antenna, cable, processing equipment required to receive time signal through GPS or from National Physical Laboratory (NPL) through INSAT shall be provided at new substations. This equipment shall be used to synchronize SAS and IEDs etc.

## **B.3.0** Substation Support Facilities

Certain facilities required for operation and maintenance of substations as described below shall be provided at new substation. In existing substation, these facilities have already been provided and would be extended/ augmented as per requirement.

#### B.3.1 Fire Fighting System

Fire-fighting system for substation including transformer and reactor shall conform to CEA (Measures Relating to Safety and Electric Supply) Regulations, 2023 as amendment time to time. Further, adequate water hydrants and portable fire extinguishers shall be provided in the substations. The main header of firefighting system shall be suitable for extension to bays covered under the future scope; necessary piping interface in this regard shall be provided. Optical Beam type heat detection for GIS hall fire protection system shall be provided for all the GIS halls.

At existing substations, the fire-fighting systems, as available, shall be augmented/ extended to meet the additional requirements.

# B.3.2 Oil evacuating, Filtering, Testing and Filling Apparatus

To monitor the quality of oil for satisfactory performance of transformers, shunt reactors and for periodical maintenance necessary oil evacuating, filtering, testing and filling apparatus would be provided at new substations. Oil storage tanks of adequate capacities for storage of transformer oil would be provided.

Online Transformer Oil Drying Out System shall be provided in line with the provisions of Standard Specification and Technical Parameters for Transformers and Reactors (66 kV and above Voltage Class) as amended up to date available on CEA website.

#### B.3.3 Illumination

Normal and emergency AC and DC illumination shall be provided adequately in the control room and other buildings of the substation. The switchyard shall also be provided with adequate illumination.

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Lighting of the entire control room building, fire-fighting pump house, other building (if any) and switchyard shall be done by LED based low power consumption luminaries.

#### B.3.4 Control Room

For new substation, substation control room shall be provided to house substation workstations for station level control (SAS) along with its peripheral and recording equipment, AC and DC distribution boards, DC batteries and associated battery chargers, Fire Protection panels, Telecommunication panels and other panels as per requirements. Air conditioning shall be provided in the building as functional requirements. Main cable trenches from the control room shall have adequate space provision for laying of cables from control room for all the future bays also.

At existing substations, the adequacy of size of control room shall be ascertained and the same shall be augmented as per requirement.

#### B.3.5 GIS Hall

The Gas Insulated Switchgear (GIS) of each voltage level alongwith other associated equipment shall be housed inside **separate** GIS building. The panels i.e. Bay level units, bay mimic, relay and protection panels, RTCC panels, PLCC panels, panels for tele-communication system etc. are to be placed in a separate room in the GIS building. The size of the room shall be such that all the panels for the bays under present scope shall be accommodated. The panel room shall be airconditioned. Further, the temperature of the room shall be monitored through substation automation system by providing necessary temperature transducers. Ventilation system of suitable capacity shall be provided for each GIS hall.

One EOT Crane of suitable capacity for erection and Maintenance of largest GIS component/assembly and all plant installed in the GIS switchgear room shall be provided in each GIS hall. The crane shall be capable of fulfilling all special requirements for erection and maintenance of GIS equipment. The capacity of the crane shall be sized to lift the heaviest GIS switchgear component.

For extension of existing GIS, existing facilities shall be suitably augmented/ extended for GIS equipment under present scope.

#### **B.3.6** Control Concept

All the EHV circuit breakers in substation/switching stations shall be controlled and synchronized from the switchyard control room/remote control center. All the isolators shall have control from remote/local whereas the earth switches shall have local control only.

## B.3.7 Visual Monitoring System (VMS) for watch and ward of substation premises:

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Visual monitoring system for effective watch and ward of substation premises shall cover all the transformers and reactors, all other major AIS Equipment (such as CB, isolators, CT, CVT, SA etc. as applicable), GIS bays, panel room, all the gates of switchyard and all entry and exit points of control room building and accordingly the location of cameras shall be decided. In addition to the gates of the switchyard, the cameras shall also be located around the boundaries at suitable locations. The camera shall be high-definition color CCD camera with night vision feature. The VMS data partly/completely shall be recorded (minimum for 15 days) at least @25fps (or better) and stored on network video recorder. The system shall use video signals from various cameras installed at different locations, process them for viewing on workstations/monitors in the control room and simultaneously record all the cameras. The VMS data should go only to the intended personnel/facility and not to the remote server of the Camera (VMS supplier).

Mouse/keyboard controllers shall be used for pan, tilt, zoom and other functions of the desired camera. The Visual Monitoring System shall have provision of WAN connectivity for remote monitoring.

All camera recordings shall have Camera ID and location/area of recording as well as date/time stamp. The equipment should generally conform to Electromagnetic compatibility requirement for outdoor equipment in EHV substation.

Advisory on deployment of CCTV issued by Ministry of Electronics and Information Technology (MEITY) shall be followed.

At existing substations, the Visual Monitoring System if available shall be augmented as per existing or better specification as required.

#### B.4 General Facilities

- a) Line Gantry/Towers are envisaged for bays under present scope only. However, for adjacent future line bay, gantry/tower shall be designed for extension (considering Hexa conductors for 765 kV and Quad conductors for 400 kV future lines) wherever applicable.
- b) Bay extension works at existing substation shall be executed by TSP in accordance with the requirement/provisions mentioned above. However, interface points shall be considered keeping in view the existing design/arrangement at the substation.
- c) TSP has to arrange for construction power and water on its own.
- d) All outdoor steel structures including anchor/foundation bolts shall be fully galvanized. The weight of the zinc coating shall be at least 610 g/m². However, for coastal/creek regions it shall be at least 900 g/m².
- e) In 765 kV and 400 kV switchyard, if spare bay of half diameter is identified as future, all

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- the equipment for Tie and Future Bay shall be designed considering the current rating of line bay i.e. 3150 A.
- f) All electrical equipment shall be installed above Highest Flood Level and where such equipment is not possible to be installed above Highest Flood Level, it shall be ensured that there is no seepage or leakage or logging of water.
- g) As per CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations 2022/CEA Manual on Transmissions Planning criteria 2023, line approaching substation shall normally be perpendicular to the substation boundary for a stretch of 2-3 km. Accordingly, TSP shall ensure that line terminations at substations are arranged in a manner to avoid hindrance to future line terminations at the substations.

## **B.5** EXTENSION OF EXISTING SUBSTATION

The following drawings/details of existing substation is attached with the RFP documents for further engineering by the bidder.

SI. No.	Drawing Title	Drawing No./Details	Rev.
			No.
A.	765/400 kV Navinal (Mundra) GIS S/s		
1.0	Single Line Diagram	The drawings shall be obtained from	
2.0	General Arrangement	the developer on finalization.	
3.0	Earthmate Layout		
4.0	Visual Monitoring System		
5.0	Bus Bar Protection		
6.0	Substation Automation		
	System (SAS)		
В.	765 kV Bhuj PS		
1.0	Single Line Diagram	0778BH_Bhuj_SWYD_E_DRG_41_001	
2.0	General Arrangement	0778BH_Bhuj_SWYD_E_DRG_42_001	
3.0	Earthmate Layout		
4.0	Visual Monitoring System		
5.0	Bus Bar Protection	GE Make	
6.0	Substation Automation System (SAS)	GE Make	

Note: Bidder is advised to visit the substation sites and acquaint themselves with the topography, infrastructure such as requirement of roads, cable trench, drainage, space availability in control rooms and LT panel room etc. and also the design philosophy.

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# SPECIFIC TECHNICAL REQUIREMENTS FOR STATCOM

The proposed STATCOMs shall be generally conforming to the requirements of CEA (Technical Standards for Connectivity to Grid) Regulations, 2007 including amendments and CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations 2022, as amended from time to time. Other CEA Regulations and MoP guidelines, as applicable, shall also be followed and complied with.

#### C.1 Introduction:

This technical specification for a STATCOM Station consists of STATCOM, MSCs (Mechanically Switched Capacitors) and MSRs (Mechanically Switched Reactors) (to be installed at MV bus) including associated coupling Transformer (rated 400/xx kV) and other equipment connected to the 400 kV bus. MV voltage level (xx kV) of the coupling Transformer can be chosen by the TSP to optimize the offered solution which meets functional requirement of this Technical Specification.

The STATCOM station shall operate asymmetrically in the leading and lagging MVAr regions as applicable to reach the dynamic range specified. The purpose of the STATCOM station is to regulate the voltage of 400 kV Bus Point of Common Coupling (PCC). The Configuration and the nominal rating of the STATCOM station is specified in this document.

The main building block of the STATCOM should be single phase Voltage Source Converter (VSC) based convertor valve (multi-level) operating in a way to eliminate or minimize AC filter requirement to High pass filter only and connected to the xx kV bus through air core reactors.

## C.1.1 Definitions and Abbreviations

For the purpose of this specification, the following definitions / abbreviations are used:

**PCC**: Point of Common Coupling (herein also called as Point of Interconnection (POI)). The connection point between the STATCOM and the ISTS at which performance requirements are defined.

Reference Voltage (Vref): The Point on the voltage/current (V/I) characteristics where the static synchronous compensator (STATCOM) is at zero output (i.e. where no reactive power is absorbed from, or supplied to, the transmission system where the voltage is controlled)

MV: Medium Voltage.

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**STATCOM Unit**: Static Synchronous Compensator based on Multi-Module technology and including air cored reactors as needed, Valve cooling, switchgear and its control and protection.

**STATCOM**: Static Synchronous Compensator consisting of STATCOM Unit(s) connected to a common coupling Transformer. A static synchronous generator operated as a shunt connected compensator, whose capacitive or inductive output current can be controlled independently of the AC system voltage.

MSC: Mechanically Switched Capacitor (Including Switchgear). A shunt-connected circuit containing a mechanical power-switching device in series with a capacitor bank and a current limiting reactor.

**MSR**: Mechanically Switched Reactor (Including Switchgear). A shunt-connected circuit containing a mechanical power-switching device in series with a reactor.

**Sub Module**: Basic single power module of a Multi Module STATCOM unit Valve. It is a Part of a STATCOM unit valve comprising controllable switches and diodes connected in full bridge arrangement, together with their immediate auxiliaries, and storage capacitor, if any, where each controllable switch consists of one or more switched valve device(s) connected in series.

Valve: Electrically and mechanically combined assembly comprising of forced commutated devices [for example insulated-gate bipolar transistor(IGBT)] assembled in levels, complete with all connections, auxiliary components, and mechanical structures, which can be connected in series with each phase of the reactor of a STATCOM unit.

**Valve Section**: Electrical assembly defined for test purposes, comprising one of several submodules.

Valve Structure: Physical structure holding valve(s), which is insulated to the full system voltage above earth potential.

**STATCOM Station**: STATCOM Station includes 400 kV Switchgear, Coupling Transformer, STATCOM, MSCs (as applicable), MSRs (as applicable) along with its switchgear and complete integrated control and protection whose outputs are coordinated. (Complete turnkey delivery at site).

CT: Current Transformer.

VT: Voltage Transformer.

**SAS**: Substation Automation System.

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**Response Time**: the duration from a step change in control signal until the voltage changes by 90% of its final change, before any overshoot.

**Settling Time**: The duration from a step change in control signal input until the STATCOM output settles to within  $\pm 5\%$  of the required control output.

**Slope**: The ratio of the voltage change to the current change over a defined controlled range of the STATCOM, normally the full (inductive plus capacitive) range at nominal voltage, expressed as a percentage.

**VSC**: Voltage Source Convertor, A forced commutated device (for example, IGBT) based self-commutated convertor that is capable of generating AC voltage from DC capacitor.

**Voltage/Current (V/I) Characteristic**: The relationship between the current of the STATCOM and the voltage at the point of connection.

**Lagging Operation**: Inductive operation or reactive power absorption of the STATCOM similar to a shunt reactor.

**Leading Operation**: Capacitive operation or reactive power generation of the STATCOM similar to a shunt Capacitor.

TSP: Transmission Service Provider

## C.2 Relevant Standard:

STATCOM Station shall comply with the following standards (latest edition):

Sl. No.	Description	Standards
1	Voltage source converter (VSC) valves for	IEC- 62927
	STATCOM	IEEE- 1052
		IEC-60747
2	Control, protection and monitoring	IEC-61000
		IEC-60255
3	Valve Hall for housing the equipment as above	1EC-60071
	comprising of:	IEC-60270
	- wall bushings for connection between	IEC-60137
	converter phases and decoupling reactors,	
	- piping and tubing connections of the cooling	
	system to converter	
	- connection of the control cabinet with the	
	converter through optical fibers	

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SI. No.	Description	Standards
	- internal lighting, auxiliary power supply (AC and	
	DC) and power socket system	
	- internal HVAC system	
4	X kV, dry insulated, air core and air self-cooled	IEC- 60076
	decoupling reactors. Mechanically Switched	
	Reactors, half-reactors stacked on above the	
	other, Outdoor installation, Complete with	
	supporting structures	
5	Power Capacitors (MSC etc.)	IEC-60871-1
6	400 kV Power transformer (Coupling Transformer)	IEC-60076
		IEC-60354
7	CT's and VT's	IEC- 61869
8	Dis-connectors and Earthing Switches	IEC- 62271
9	HV and MV Circuit Breakers	IEC- 62271
10	Surge Arresters	IEC- 60099
11	Auxiliary and grounding transformer	IEC- 60076
		IEEE C57.32
		IS- 5553 (Part 6)
12	Neutral Grounding Resistor, charging resistor	IEEE- C57.32
13	UPS, SMPS and Other Power supply units	IEC- 62040
		IEC- 61558
14	Cyber Security	IEC-62243

#### C.3 Scope of work for STATCOM

The scope of work with regard to the works associated with the STATCOM shall comprise ±300 MVAr Modular Multi-level Voltage Source Converter (MMC-VSC) based STATCOM along with 2x125 MVAr MSC (Mechanically Switched Capacitors) and 1x125 MVAr MSR (Mechanically Switched Reactors).

STATCOM can either be Single/ multiple units. The minimum size of a unit allowed is 150 – 200 MVAr. TSP shall ensure that there are no coordination issues between multiple STATCOM branches of STATCOM station. Further complete Dynamic range for STATCOM may also be installed based on appropriate studies instead of combination of VSC with MSC/MSR technology. Minimum MV bus voltage is to be decided by OEMs.

The TSP shall be responsible for the complete installation of STATCOM station along with the substation works as specified in the complete scope of work.

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The TSP shall also perform the system studies (steady state and dynamic) according to the requirement mentioned and documentation of the same shall be preserved by TSP and to be submitted to CEA/CTU/GRID-INDIA, as per their request.

TSP shall carry out a detailed study on prevailing system conditions before interconnection of the STATCOM to assess the performance of the STATCOM. Parameters tuning to avoid any adverse impact on the grid with integration of the STATCOM shall also be identified and implemented at this stage. TSP shall carry out tuning of Power Oscillation damping (POD) along with an interaction study with nearby HVDC/FACTS controllers.

TSP shall ensure interconnection study at the time of commissioning and shall also be responsible for tuning the POD during the license period as per relevant standards (e.g. IEEE 1052).

The switchgear for connection of STATCOM units, MSCs and MSRs provided on the secondary side of the coupling transformer shall be of standard voltage rating as per relevant IEC. The switchgear, structure, control, protection and substation automation on the 400 kV side shall be as per applicable Technical Specification of the substation equipment.

Generally, the purpose of STATCOM is to improve system stability, provide damping, and smooth out the step voltage change associated with MSCs, MSRs and external compensating equipment (i.e. any existing capacitor and reactor banks) switching and provide steady state VARs as needed to support the 400 kV bus voltage.

In order to get optimum control of MVAr, the control of MSCs and MSRs, as well as reactor banks connected on the 400 kV HV side, may be integrated along with STATCOM control to provide steady state 400 kV bus voltage control in a smooth manner. MSRs and MSCs are to be switched to relieve the STATCOM from high level operation, reduce its continuous losses and maximize its dynamic control potential. There should be a provision for the independent operation of MSC/MSR after delinking it with STATCOM controls when STATCOM is out of service due to any reason. Switching of MSC/MSR shall be based on value of external bus voltage.

The operating functions of the STATCOM Station shall include:

- Steady state voltage control of 400 kV bus,
- Balance steady state voltage at 400 kV bus,
- Dynamic over-voltage control,
- Transient and Dynamic stability control

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Damping of Power Oscillations

It is assumed that the arresters will limit any transient and switching surge over voltages and may also, by design, limit dynamic over voltages.

The requirement of reactive power compensation (as defined above) guaranteed by the TSP shall not be less than the levels specified considering following.

- The total cumulative Capacitive (+) and Inductive (-) MVAr rated Capacity of STATCOM Station as defined above comprising of STATCOM, MSCs (as applicable), MSRs (as applicable), coupling transformer, coupling reactor or any filter (if applicable) shall be rated at 1 p.u. voltage, 1 p.u. frequency and 50 ° C (Celsius) ambient temperature at 400 kV Bus (Referred to as "Point of Common Coupling" or PCC).
- Capacity of one or more branches of MSC, MSR in STATCOM Station can be included in the STATCOM with equivalent capacity. Accordingly, ratings of STATCOM Unit/Branch equipment may be designed.

Example of equivalent acceptable solutions for each STATCOM Station is given below:

## For ±300 MVAr STATCOM:

**Option 1**: ±300 MVAr STATCOM, 2x125 MVAr Mechanically switched Shunt Capacitor (MSC), 1x125 MVAr Mechanically switched Shunt Reactor (MSR).

**Option 2**: +425/-300 MVAr STATCOM, 1x125 MVAr Mechanically switched Shunt Capacitor (MSC), 1x125MVAr Mechanically switched Shunt Reactor (MSR).

**Option 3**: +300/-425 MVAr STATCOM, 2x125 MVAr Mechanically switched Shunt Capacitor (MSC).

**Option 4**: ±425 MVAr STATCOM, 1x125 MVAr Mechanically switched Shunt Capacitor (MSC)

Option 5: +550/-300MVAr STATCOM, 1x125 MVAr Mechanically switched Shunt Reactor (MSR)

Option 6: +550/-425 MVAr STATCOM

 The rated capability of STATCOM, MSC (as applicable) and MSR (as applicable) shall be at 400 kV (Referred to as "Point of Common Coupling" or PCC) and in the steady state frequency range of 48.5 Hz-50.5 Hz.

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- The STATCOM Station including STATCOM Units, MSCs and MSRs shall be designed to operate continuously under the worst possible combination of steady state voltage range of 360-440 kV and frequency range of 47.5 Hz 52.5 Hz respectively and transient and temporary over voltages defined in Clause C.6.1-f).
- The AC voltage unbalance at fundamental frequency shall be assumed equivalent to a negative phase sequence component of 1.5% for equipment rating purposes.
- The reactive power compensation levels shall be determined by manufacturing tolerances of the components and measurements carried out using metering accuracy instrumentation at the 400 kV feed points to the STATCOM Station.
- The reactive power capability shall also be determined by calculations based on test values of appropriate quantities at the discretion of the owner.
- In calculations of capability and availability, the owner shall assume the most unfavorable combinations of control, manufacturing and measurement tolerances.
- In case more than one STATCOM Station are installed in a particular substation, each STATCOM Station shall be connected to 400 kV bus individually with complete separate downstream system. Each individual STATCOM station shall have complete independent yet coordinated control system to avoid simultaneous tripping of both STATCOM Stations. The system shall be design in such a way that single common contingency (other than loss of 400 kV voltage, abnormal system events) will not cause tripping of both STATCOM Stations.
- Operation of STATCOM Station shall not excite any resonance condition in connected Power System.
- Control of STATCOM Station shall be designed to prevent hunting between MSRs, MSCs and STATCOM.

## C.3.1 STATCOM building

The STATCOM station shall have an independent building including a separate control room different from the main control room building of the 765/400kV Substation.

The STATCOM Building shall comprise of following facilities:

- 1. Control and Relay Panel room
- 2. ACDB and DCDB room
- 3. Battery room
- 4. Service Room cum workshop
- Conference room
- 6. Valve hall
- 7. Cooling system room

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- 8. Lobby
- 9. Corridor with minimum width of 1600 mm
- 10. Portico
- 11. Common Toilet
- 12. Provision of shaft for electrical, sanitary, water supply facilities
- 13. Other facilities as per functional requirement of building
- 14. AHU Room

# C.4 Ambient Condition

STATCOM Station should be designed to perform at 50 degrees C ambient temperature.

# C.5 Power System Characteristic

The following AC power system characteristics apply at the point of connection i.e. point of common coupling in this case (PCC). STATCOM station operation is required within the parameter value and duration given in following table:

S. No	Power System Characteristic	Value	unit
1.	Nominal ac system voltage, line-to-line	400	kV
2.	Maximum continuous ac system voltage, line-to-line	420	kV
3.	Minimum continuous ac system voltage, line-to-line	380	kV
4.	Maximum short-term ac system voltage, line-to-line	448	kV
5.	Maximum duration of item 4	10	s
6	Continuous negative-sequence voltage component (used for performance calculation)	1	%
7	Continuous negative-sequence voltage component (used for rating calculation)	1.5	%
8	Continuous zero-sequence voltage component	1	%
9	Nominal ac system frequency	50	Hz
10	Maximum continuous ac system frequency (for rated output)	50.5	Hz

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S. No	Power System Characteristic	Value	unit
11.	Minimum continuous ac system frequency (for rated output)	48.5	Hz
12.	Maximum short-term ac system frequency	52.5	Hz
13.	Minimum short-term ac system frequency	47.5	Hz
14.	Basic Insulation Level (BIL)	1550	kV peak
<b>1</b> 5.	Switching impulse level (SIL)	1050	kV peak
16.	Power Frequency Withstand voltage	630	kV
17.	Maximum three-phase fault current		
i	a) for performance requirements	a) 63	kA
	b) for rating of STATCOM	b) 63	kA for 1s
	X/R (Positive/Negative Seq)*	23.5	
	X/R (Zero Seq)*	23.6	
	Clearing time - normal	0.1	S
	Clearing time – backup	0.75	S
18.	Maximum three-phase fault current	63	kA
19.	Minimum three-phase fault current #		
i	-for performance requirements	29	kA
	-for safe operation	29	kA
20.	Maximum single-phase fault current	63	kA
21.	Minimum single-phase fault current#	8	kA
22.	Harmonic impedance sectors for each harmonic number up to the 49th harmonic or system impedance data as R-X values with frequency steps not larger than 1 Hz (for performance and/or STATCOM system component rating)	Chapter 7.3 Publication 13	of CIGRE
23.	Background harmonic voltage (or current) spectrum (for STATCOM components rating) (Distortion up to 15th Harmonic	5th Harmonic 1.5% 7th Harmonic 1.0% Other Harmonics 0.5%	

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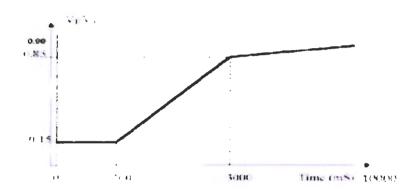


S. No	Power System Characteristic	Value	unit
		(each)	
24.	Power System Phase Rotation	C	CW

#Calculated considering outage of 2 nos. 765/400 kV ICTs at Navinal S/s and 400 kV and 765 kV Sectionalisers under closed condition as per the approved scheme.

The STATCOMs shall remain connected to the grid and shall be able to operate at rated reactive power capability when voltage at the interconnection point, on single phase or three phases dips up to the level depicted by the thick lines in the following curve (for specified time) and up to at least 0.3 p.u. in case of two phase faults:

VT: Actual Voltage; Vn: Nominal Voltage



## C.6 STATCOM Station Characteristics

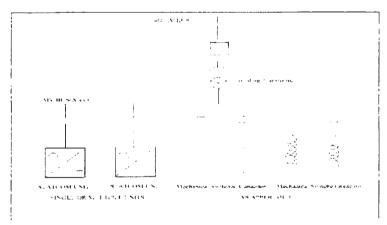


Figure-1: Conceptual Indicative Schematic diagram of STATCOM Station

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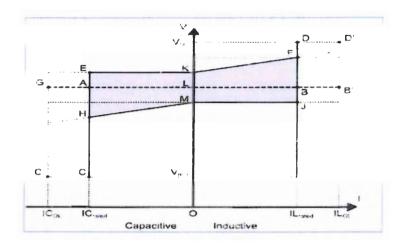


Figure-2: VI Curve of the VSC Portion

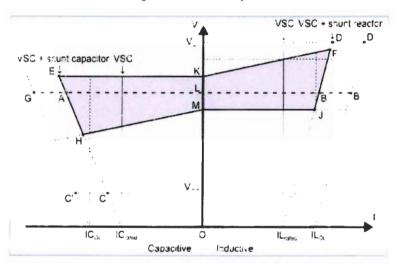


Figure-3: VI Curve of the STATCOM Station

# C.6.1 STATCOM Station Ratings

The output of a STATCOM Station shall be adjusted continuously over the range illustrated in Figure-3.

The following items define the ratings of the STATCOM station equipment.

a) The STATCOM Station should regulate the 400 kV bus voltage to a reference voltage of 400 kV (1.0 per unit, Point L Figure-3), continuously adjustable between 0.95 per unit and 1.05 per unit.

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- b) The nominal capacitive and inductive reactive power output of the STATCOM should be as defined in the scope, at 1.0 pu AC bus voltage and nominal system frequency f, and 50°C ambient temperature (Point A and point B of figure-2).
- c) The slope of the STATCOM Station characteristic should be adjustable in steps of not greater than 0.5% between 1% and 8%, on a basis of cumulative MVA capacity of STATCOM Station (A+B in Figure-3).
- d) The STATCOM Stations shall continue to inject reactive power during temporary under voltage down to 60 kV (0.15 p.u.) for the duration 0.3 sec (Point C) and STATCOM behavior for voltages above 0.15 p.u. shall be as specified under section C.5 above, ; the STATCOM system may be tripped (or blocked) if the under voltage persists for time beyond limits specified under section C.5 above.
- e) The STATCOM shall continue to absorb reactive power during HVRT Conditions in a controlled manner as per the following.

Nominal Voltage (pu)	Minimum time for remaining connected to the Grid
V > 1.50	Instantaneous trip
1.50 ≥ V > 1.30	100 milli seconds
1.30 ≥ V > 1.10	10 seconds
V ≤ 1.10	Continuous

STATCOM Station may be tripped if the respective temporary over voltages as mentioned above persists for more than its respective mentioned duration.

- f) The STATCOM Station should be capable of repeating temporary operation as defined in any one of item (d) and (e) as above for at least 3 charging cycles in 60 mins.
- g) The coupling transformer and all bus equipment, such as filter branches (if applicable), MSC and MSR branches etc. and the MV Bus should be rated to withstand the specified continuous and short-term operation, and to withstand or be protected against voltage and current stresses that exceed these conditions.
- h) All equipment in the STATCOM Station should be capable of sustaining, without damage, any fault limited by the maximum design short circuit level of the system and the Coupling transformer impedance
- i) The TSP shall assume the negative sequence voltage of 1% at rated short circuit level and provide control to reduce this unbalance.
- j) The injected harmonics by STATCOM Station under the full operating range measured at 400 kV Bus (PCC) in accordance with IEEE Standard.

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- k) The STATCOM controls should be designed to correct negative sequence voltage during steady state operation.
- The switching module design should include an appropriate allowance for stray capacitance and component tolerances.
- m) The STATCOM should be designed to prevent, or alternatively to withstand, false firing events, i.e., the firing of any valve at an incorrect time in the cycle or when not ordered.

#### C.6.2 Control Objectives

The control system shall control the STATCOM, MSCs, MSRs required under this specification, as well as all bus reactors on the 400 kV HV bus of the substation.

Operation logic for the breakers, disconnectors and earth-switches in the STATCOM Station shall also be incorporated in the control system. The control shall be programmable and shall have sufficient scope and flexibility (software programming margin of at least 20%) to permit re-programming according to future changes/addition in the power system. The operator interface must be integrated in a latest version of Windows environment.

## C.6.2.1 STATCOM Station Functions and Applications

## C.6.2.1.1 Voltage Control mode (Automatic and Manual)

Control of the positive sequence component of the fundamental frequency voltage in steady state at POI shall be , with slope in the range as specified at clause 6.1 c) above.

There shall be following provisions in STATCOM System to operate in Voltage Control Mode:

- a) To adjust the reference voltage for changes by Grid operator.
- b) To adjust the value of reactive power droop in pu to provide a stable, coordinated and dynamic response.
- c) To adjust the voltage dead band with a minimum magnitude of ±0.05pu

#### C.6.2.1.2 Fixed Reactive Power Mode

In this mode, the STATCOM system shall maintain a specified constant reactive power output at the POI under continuous / steady state operating region. The target reactive power level and mode (injection or absorption) shall be specified by the Grid operator. There shall be a provision to adjust the reactive power set point. The dynamic response of the STATCOM system to any changes in reactive power shall be positively damped with a damping ratio of 0.3 or better.

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## C.6.2.1.3 Steady State Condition

The STATCOM Station (STATCOM along with MSCs and MSRs) shall provide necessary reactive power support to the 400 kV bus (PCC) to compensate for voltage variation under steady state.

## C.6.2.1.4 Dynamic Over-voltage Control Performance

The STATCOM shall be required to provide necessary reactive power support with fast and smooth variation so that over-voltages under dynamic conditions are controlled. STATCOM shall smooth out the step caused by the switching of MSCs and MSRs.

The operation of each STATCOM over its range of MVAr from full capacitive to full Inductive capacity and vice-versa shall be on the basis of smooth variation.

# C.6.2.1.5 Transient and Dynamic Stability Performances

The STATCOM Station shall provide necessary reactive power so that the transient and dynamic stability of the Owner's system is enhanced.

#### C.6.2.1.6 Damping of Power Oscillations

The STATCOM shall provide necessary damping to power oscillations by modulating its output in its entire range based on the measured rate of change of power/frequency at the 400 kV bus. The damping controller would track local area oscillations as well as wide area oscillations and control would include several loops each focused on different frequencies.

TSP shall ensure the damping of oscillation during the entire license period including the pre-commissioning period as per relevant standards. (e.g. IEEE 1052).

#### C.6.2.1.7 Facility for compensation of phase imbalance

Provide negative phase sequence voltage control to minimize the presence of negative sequence content of the 400 kV bus voltage.

#### C.6.2.1.8 Start up and Initial Switching

The operation of STATCOM Station during start-up/initial switching on should not create significant energizing transients causing voltage drop, voltage distortion and swinging of transmission voltage angle at the PCC bus by more than +/-5%. TSP shall have to ensure this analytically during the design phase and also in the field after the commissioning of the facility. TSP shall prepare the design documentation and the same shall be preserved by TSP and to be submitted to CEA/CTU/GRID-INDIA, as per their requirement.

## C.6.2.1.9 Gain Supervision and Control

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To control the regulator gain in order to prevent oscillations and excessive overshoot in the STATCOM response, a gain supervision function shall be implemented. This shall be an essential function for the supervision of stability of closed-loop voltage control. The function of this controller is that when the supervision of the gain in the voltage regulator detects oscillations in the voltage controller output, the gain shall gradually be reduced until stability is reached. Normally it is a changed condition in the transmission system contribution to the closed loop gain that results in instability. The reduction in the voltage regulator gain shall only balance the external change. The control should be adaptive in order to maximize its effectiveness. Gain reductions should be indicated and the reduction of the gain shall be able to be reset to nominal value by means of commands from the operator interface or automatically. A relative gain factor shall also be able to be changed from a gain optimizer.

# C.6.2.1.10 Coordinated reactive power control of external devices

To optimize the use of dynamic VARs versus steady state VARs, control of externally connected shunt capacitor or reactor banks shall be implemented. Such banks will be connected locally to a HV bus or/and at MV bus. For simultaneous control with the supplementary VSC current controller, coordination for the two functions shall be provided. External devices like Mechanically Switched Capacitors (MSC)/Mechanically Switched Reactors (MSR) can be switched ON or OFF to position the steady state operating point of the VSC so as to extend its dynamic range. There should be a provision for independent operation of MSC/MSR after delinking it with STATCOM controls when STATCOM is out of service due to any reason. The threshold values for switching the MSC/MSR on/off shall be configurable in all modes of operation.

# C.6.2.1.11 Supplementary VSC current controller

To optimize the use of dynamic VARs versus steady state VARs, a control function that slowly reduces or offsets the STATCOM point of operation shall be implemented. By deliberately adjusting the voltage reference setting within a narrow window the STATCOM system output is pushed towards either a specific point or towards a window to preserve dynamic range. This slow operating function is meant to provide for slower controllers, such as externally connected shunt banks to operate and meet the slower long term voltage variations caused by daily or weekly load variations. Rapid changes in the system voltage that call for dynamic compensation will have priority over this type of controller.

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#### C.6.2.1.12 Gain optimization

To provide operation at optimal regulator gain, a fully automatic optimizing function shall be implemented. This function operates by inducing a small change in the STATCOM output. The gain is adjusted based on the network response signal.

#### C.6.2.1.13 Control of Direct Current

During STATCOM operations, any flow of direct current to the transformer's MV side must be less than 25% of the transformer magnetizing current. DC current flow in the transformer should be minimized by an independent control function that minimizes DC current. For presence of up to 0.2% second harmonic in 400 kV system, the STATCOM control should minimize DC current flow in the transformer.

#### C.6.2.2 Under Voltage Strategy

It is essential that the STATCOM Station operates in a robust manner when transmission system under voltages appears. In case of single phase or three phase faults, the STATCOM units must operate unrestricted, producing its rated capacitive current for transmission system voltages down to 0.15 p.u. In case of two phase fault, STATCOM shall be capable to produce rated capacitive current atleast down to 0.3 p.u, however, it shall be designed to operate upto 0.15 p.u. The STATCOM must be designed to operate at transmission system under voltage, even considering that severe voltage unbalances can appear. The STATCOM must not be restricted by short term negative sequence voltages up to 1.5%, appearing in conjunction with under voltages.

Transmission system under voltages below 0.15 pu will appear in conjunction with transmission system faults. The STATCOM must ride through during faults and post fault under voltages. The minimum trip delay for the STATCOM Station, upon complete loss of the transmission system voltage shall not be less than 5 seconds. If station AC auxiliary power distribution is affected, critical loads must be fed from DC station batteries, uninterrupted power supply (UPS) without tripping the STATCOM Station. Adequate capacity must be kept in DC station batteries, UPS to feed critical loads for the smooth operation of the STATCOM Station facility. There must be redundant station battery system with each station battery system capable of delivering 100% load.

At under voltage conditions for the transmission system voltage, special control strategies are activated which override the normal control modes presented above. Normally if the voltage is low, the output from the STATCOM will be capacitive. If the voltage in all three phases goes below a level, but not greater than 0.15 pu, a special under voltage strategy may be activated that controls the STATCOM output to 0 MVAr. As soon as the voltage goes

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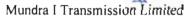
higher than 0 0.15 pu, the under voltage strategy is deactivated and the normal control will be in operation (for the specified duration).

The STATCOM Station must not be tripped or shut down automatically due to under voltages appearing for specified duration as specified under section C.5 above. STATCOM Station must continue to operate when AC system Voltage on any or all phases dips down to 0.15 pu voltage as per the characteristic given at section C.5.

# C.6.2.3 Over Voltage Strategy

- C.6.2.3.1 The TSP shall carry out dynamic stability study upfront in order to assess the dynamic overvoltage requirements. These studies shall include conditions with maximum and minimum short circuit system MVA conditions, single phase and three phase faults as well as stuck breaker, outage of the nearby generator and also with the outage of parts of the STATCOM Station. It is important that the STATCOM Station rides through temporary over voltages and not trip when it is needed the most.
- C.6.2.3.2 The system should be able to withstand any 3 phase, 5 cycle (100 ms) and single phase 10 cycles (200 ms) fault with consequent loss of a 400 kV double circuit line and loss of a 500 MW generator. The fault duration mentioned above corresponds to time assumed for the persistence of fault. For other system parameters refer clause 5 above (Power System Characteristics). In addition to above requirement, system contingency cases as provided in Annexure-I need to be considered and satisfied.
- C.6.2.3.3 The 400kV system and equipment to which the STATCOM Station is connected is designed to withstand switching surge overvoltage up to 2.5 p.u. and power frequency over voltages up to 1.5 p.u. with initial value of the temporary overvoltage up to 2.0 p.u. for 1-2 cycles. Based on arrestor coordination and under the worst case scenario the 400 kV system phase to ground peak over voltages may be expected as follows
  - i) 650 kVp for 3 peaks
  - ii) 575 kVp up to 5 cycles
  - iii) 530 kVp up to 1 second
  - iv) 475 kVp up to 10 seconds
  - The STATCOM Station shall be designed to withstand these sequential over voltages.
  - b) If the over voltages greater than 1.1 p.u. are exceeded in magnitude and duration due to any system contingencies, suitable control action shall be taken by STATCOM Station to bear this kind of contingency.

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- c) The TSP shall evolve the insulation co-ordination of the components of the STATCOM Station after studies have been conducted to determine the over- voltage profile with the STATCOM connected to the system.
- d) The TSP shall ensure that STATCOM Station will not excite ferro-resonance and subsynchronous oscillation in the AC system. The study report in this regard shall be preserved and to be submitted to CEA/CTU/GRID-INDIA, if required.
- e) It may also be noted that the tripping action for 400 kV lines is initiated if the overvoltage exceeds 1.1 p.u. for 10 seconds. The tripping of 400 kV lines is initiated if 1.5 p.u. voltage persists for more than 100 milli seconds. The over voltage strategy shall be coordinated with these settings such that the STATCOM Station rides through up to these levels.

# C.6.2.4 STATCOM Station Over load / Over Current

The overvoltage cycles mentioned in clause 6.2.3.3 above create a corresponding current overload in the STATCOM Station components; the STATCOM Station and its components shall be designed to withstand these.

In addition to the above the STATCOM Station and its components shall be designed to withstand overloading caused due to the following eventualities.

- i) Short circuits and ground faults in the 400 kV system especially those occurring near the STATCOM Station and medium voltage bus of the STATCOM Station.
- ii) Transient overvoltage due to switching operations and atmospheric effects.
- iii) Temporary over voltages.
- iv) Short circuits in the transformer secondary circuit such as:
  - Bushing terminal fault
  - Flashover across a reactor, Bus Bar and other connected components/switchgear etc.
- v) Protection system faults.

If the rated overvoltage is exceeded as a result of prolonged stressing or for other reasons, the protection specified elsewhere in the specification shall come into effect to prevent damage.

#### C.6.2.5 Dynamic Performance Controls of STATCOM Station

The TSP must describe in detail, the dynamic reactive power controls for enhancing stability margin and also damp oscillations of any critical frequencies. The dead band for continuous damping control must be very small so that there are no discernible sustained oscillations.

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#### C.6.2.6 Protective Control Functions

The TSP shall provide all necessary protections including Main and Back-up protections for all protective zones and equipment like transformers, STATCOM Units, MSCs (if applicable), MSRs (if applicable), MV Bus Bar etc. TSP shall provide any protective control functions to meet the performance requirement of STATCOM under the scope of the TSP.

## a) Overvoltage Protection

The TSP shall provide adequate overvoltage protection as a result of any normal operation, mal-operation or system event.

# b) Over current Protection

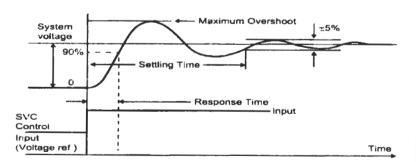
The TSP shall provide adequate over-current protection for the STATCOM Station as a result of any abnormal operation, mal-operation or system event.

## c) Gate level control Supervision

The TSP shall provide adequate Sub module Gate level control supervision.

## C.6.2.7 STATCOM Station Response

STATCOM station response shall be such that the change in measured system voltage to small disturbance should reach 90% of the desired total change within 30 msof initiating a 5% step change of voltage reference. The maximum overshoot should not exceed 120% of the total change and the settling time should not exceed 100 ms, after which the voltage should be within ±5% of the final value. This response characteristic within these limits must be respected when the system's three-phase fault MVA is between the minimum and maximum value defined in clause-5. The response of the system voltage using the actual controller should be validated on a real time simulator during the factory acceptance test (FAT) at the manufacturer's premises. For the purpose of STATCOM Station, response time measurement and signal conversion of the voltage, the error should not exceed 0.3%. The voltage response acquisition circuit should have a response time of no longer than 10 ms. However, time longer than 10 ms can be allowed provided the requirement of STATCOM response time is met.



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Figure-4 Response and Settling time

## C.6.3 Harmonic performance and AC harmonic filter design

It is likely that with multi-level VSC based technology, no filters or only a small high-pass filter will be needed. The STATCOM shall be operable without AC filters. The STATCOM Station should be designed to eliminate the effects of any harmonic resonance between its MSRs, MSCs banks, filter branches, and the AC system. To limit the harmonic distortion imposed on the 400 kV transmission system, the additional contribution of harmonic distortion from the STATCOM Station to 400 kV system (PCC) should not exceed 1% for the total and 0.5% for any specific harmonic.

#### C.6.3.1 Filter performance

The distortion levels as specified should be met for the following:

- a) The continuous range of all system and environmental conditions.
- b) Variation in total filter capacitance due to manufacturing tolerance, ambient temperature, aging, and changes in capacitance up to alarm level.
- c) Variation in tolerance for STATCOM parameters, such as transformer winding unbalances, valve firing variations MSC and MSR unequal reactor and capacitor reactance between phases.
- d) System frequency in the range of 48.5 Hz to 50.5 Hz. Calculation should take into account all possible combinations of STATCOMs, MSCs and MSRs.

# C.6.3.2 Filter Component rating

The harmonic filter components (and other STATCOM components) should be rated to carry continuously the harmonic currents caused by the background harmonic distortion of the system and the harmonic currents produced by the STATCOM itself. Unless otherwise specified, harmonic currents from the system and the STATCOM of the same order should be added arithmetically. All filter harmonic currents of different order should be added quadratically (root sum of squares).

The rated voltage of capacitors should be derived from the largest arithmetic sum of the power-frequency and individual harmonic voltages obtained from stress calculations in continuous operating conditions (Note: Maximum fundamental voltage and maximum harmonic contributions may not exist at the same time for STATCOM configurations including MSRs or MSCs).

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For filter capacitor voltage rating, the loss of capacitor unit or elements should be considered up to the trip level.

The rated voltage of so-called "low voltage" capacitors (e.g. in double or triple tuned filters) should be chosen such as to also withstand imposed transient stresses from faults, energization, or other switching events.

#### C.6.3.3 Harmonic at PCC

The STATCOM Station's contribution to the harmonic distortion levels at the STATCOM Station connection point (PCC) to the transmission system shall not exceed the limits defined in IEEE-2800 standard.

## C.6.3.4 Harmonic calculation:

Chapter 7.3 of CIGRE Publication 139 together with information in PSSE network files given shall be used for the Network harmonic impedance.

#### C.6.4 MV Switchyard

- Medium Voltage (MV) delta bus shall be grounded through a Grounding Transformer
   (i.e. zig-zag winding Transformer) along with a suitable resistor in the neutral.
- MIV Switchyard of different STATCOM Station branches shall be fenced with a fence height of 3 meter. To minimize the probability of electrical fault suitable arrangement i.e. electrified fence shall be done to prevent the encroachment of unwanted animals or other to minimize the probability of electrical faults (Ph-E, Ph-Ph). Further bus bar arrangements shall be made in a way to minimize the probability of electrical faults.
- Secondary side of the Coupling Transformer shall be provided with suitable surge capacitors to mitigate transfer surges.
- For MV bus bar, an Aluminum conductor (Tube, Rectangular Hollow Section or C Section)
  may be used, however, a suitable bus bar end cover/cap shall be provided to avoid any
  animal/bird entering the hollow space.

#### C.6.5 Broadband Interference

## C.6.5.1 Radio Interference

The TSP shall take necessary precautions in the form of shielding of valve hall and building or Containers to meet its own requirement together with any requirements that may be specified in Section-Project. Further, the following requirements shall also be met:

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- a) With the STATCOM Station operating at any load upto rated value and within the design range of firing angle, the radio interference level from electromagnetic or electrostatic inductions generated by the STATCOM station shall not exceed 100 micro-volts/m, under fair weather conditions, at 500 m away from STATCOM fence or boundary of the substation whichever is higher. The Radio Interference Level (RIL) criteria shall be achieved at all frequencies within the range of 150 kHz to 300 MHz and with the STATCOM operation at any level up to and including rated value, the design shall provide correcting measures, in case the specified design is not being realized in the final installation. In case of any third-party complaints about the radio interference, suitable measures shall be implemented by the TSP
- b) Measurements of actual RI at STATCOM Station shall be made by the TSP, at points along the above defined contour and at other critical points.
- c) RIV (Radio Interference Voltage) measured at a phase to ground voltage (266 kV rms) in accordance to NEMA-107 shall not be more than 500 micro-volts for 400 kV system. For other system voltages, IEC/NEMA in the order of preference shall be applicable.

## C.6.5.2 Interference with Power Line Carrier and Open Wire Carrier system

The TSP shall take the necessary precautions in the form of noise suppression techniques and filtering devices to prevent harmful interferences from STATCOM Station to the power line carrier communication (PLCC) system operating on connected AC transmission network.

The frequency spectra to be protected are:

System Frequency spectrum

Power Line carrier 30 kHz to 500 kHz

Open wire carrier 5 kHz to 30 kHz

## C.6.6 Audible Noise

The TSP shall limit the audible noise in various areas of the STATCOM Station buildings and containers to the following values.

Valve hall (Inside)	90 dBA
Mechanical equipment areas indoor (measured at 2 meter distance)	75 dBA
Mechanical equipment outdoor (Measured at 15 m distance)	75 dBA
Control Room Building*	60 dBA
At the limits of the STATCOM STATION perimeter fence	

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\*This is the background noise from the ventilation system in adjacent rooms, control cubicles etc. Printers, recorders may be switched off during the measurement.

## C.6.7 Loss Requirements

- C.6.7.1 The TSP must guarantee the total losses of STATCOM Station, be less than 1% of the reactive power output individually at its inductive limit (STATCOM+MSRs) and capacitive limit (STATCOM+MSCs) for the cumulative highest reactive power output of STATCOM Station at PCC with the worse combination of manufacturing tolerances for the Option-1 to 4 as provided in clause C.3. In case of Option 5 as provided in clause C.3 i.e. +550/-425 MVAr STATCOM without MSC and MSR, the TSP must guarantee the total losses of STATCOM Station will be less than 1.5% of the reactive power output individually at its inductive limit and capacitive limit for the cumulative highest reactive power output of STATCOM Station at PCC with the worse combination of manufacturing tolerances. For the purpose of total loss measurements, it should be assumed that the ambient temperature is 20 °C, the PCC voltage is 1 per unit, and the slope setting is 1%. The STATCOM system may not operate under these conditions, but they provide a common base.
- C.6.7.2 The total losses shall include all components, as well as different parts or subsystems of the complete STATCOM Station such as coupling transformer, All VSC systems and components, MSC and MSR, Control and protection systems, including ancillary devices such as HMI, fault recorders, and SCADA, Auxiliary Power supply systems, cooling systems, Building ancillary services such as lighting, air conditioning, heating, and ventilation. It may be noted that for the redundant VSC valve levels and dual/redundant control and protection systems, the losses of redundant VSC valve levels and dual control and protection systems shall be considered during loss measurement.
- C.6.7.3 For the dual or redundant systems design of STATCOM Station, such as dual pumps or redundant fans, dual systems losses are to be excluded, if the dual system is not in service during the normal operation of the STATCOM Station. However, dual systems should be included if they are required to be in service under the defined operating conditions. The same methodology shall be applied for HVAC (heating ventilation and air conditioning systems).
- C.6.7.4 The TSP is required to prepare documentation for the detailed calculation of total losses based on measurement during Factory Acceptance Tests of major equipment and systems mentioned above as per relevant IS/IEC/IEEE standards and the same shall be preserved and to be submitted to CEA/CTU/GRID-INDIA, as per their requirement. Further for equipment/systems, whose loss measurement cannot be done during Factory Acceptance Test, the same can be measured at the site, and a combination of calculation and

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measurement shall be used to derive the total losses as specified above. During Loss measurement, all fans, and pumps; valve room and control room air-conditioning system shall be switched on. However, redundant fans, pumps and air-conditioners shall be kept off during loss measurement.

C.6.7.5 During the factory tests the losses for the following equipment shall be measured/ assessed as detailed below:

# Coupling transformer:

Losses shall be measured at factory/lab at the maximum rating, at power frequency as per relevant IEC/IS under below mentioned conditions:

- i. No load loss (Iron loss) at rated voltage and fundamental frequency.
- ii. Load loss (copper loss) at rating corresponding to maximum continuous current and at 75 °C.
- iii. Transformer cooling equipment's loss (Auxiliary loss) at rated voltage and fundamental frequency.

#### Reactors:

The losses shall be measured at the factory/lab at the maximum rating at power frequency as per relevant IEC/IS.

#### **VSC Valves:**

Converter losses comprise the losses in power electronic switches [insulated gate bipolar transistor (IGBT) or equivalent], made up of conduction and switching losses, and the losses in DC capacitors, resistors, and inductors used within the converter system. Refer IEEE-1052 for calculating VSC losses.

# Capacitor:

The capacitor losses shall be measured at the manufacturer's works at power frequency as well as calculated to obtain the losses in the complete bank on the basis of factory measurement.

# **Auxiliary System:**

Aux. power losses shall be calculated from the kW and efficiency of all motors (name plate rating) of the cooling system, air conditioning, ventilation etc. The higher of the total losses

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for the entire auxiliary systems occurring at full capacitive capacity MVAr or full Inductive MVAr as the case may be shall be considered for arriving at the total losses.

# Harmonic Filters, if any:

The losses shall be calculated at the maximum STATCOM Station loading at 400 kV and 50 Hz.

The calculations shall be on the basis of the tested results of the components.

#### C.6.8 Selection of Insulation Levels

#### C.6.8.1 Arresters:

Protective levels of arresters connected to the 400 kV AC Bus Bars of the STATCOM Station shall be coordinated with the insulation and surge arrester Characteristics of the 400 kV AC systems to which the STATCOM Station is to be connected. The specification and characteristics of the surge arresters installed in 400 kV AC system is given in the Substation specifications. The front of wave (FWWL), lightning impulse (LIWL) and switching impulse withstand levels (SIWL) shall be determined by the following margins:

- a) A SIWL at least 1.15 times the switching impulse protection level.
- b) A LIWL which is an IEC standard level corresponding to the SIWL and shall be at least 1.25 times the lightning impulse protection level.
- c) A FWWL which is at least 1.25 times the front of wave protection level.

In addition to the above minimum basic requirement, the various insulation level of 400 kV equipment shall be as below. The STATCOM Station equipment, coupling transformers etc. shall be co-ordinated accordingly.

Description	SIWL	LIWL
All equipment including Transformer Bushing and	1050 kVp	1425 kVp
winding		

### C.6.8.2 Valves

The requirement of insulation levels of the valves shall be as per the design requirement.

### C.6.8.3 Air clearances

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The air clearances shall be determined by the TSP based on the required withstand levels for all waveforms in order to limit the probability of flashover within the STATCOM Station to a target value of one flashover in 15 years.

### C.6.8.4 Switchyard

The air clearances for switchyard equipment shall be equal to or greater than the minimum values as specified in IEC-60071. Altitude correction factor (if any) shall also be considered as per IEC.

### C.6.8.5 Leakage distances

The Creepage/leakage distance across insulation shall be determined by the TSP and shall be adequate to ensure that under conditions of heavy pollution, the probability of a flashover of an insulator does not exceed one in 15 years. However, the leakage distance for all AC insulators for outdoor installation shall not be less than 31 mm/kV of the maximum operating phase to earth rms voltage at the insulator. The leakage distance of equipment connected to 400 kV systems shall not be less than 13020 mm.

Specific creepage distance for outdoor bushings, insulator strings and long rod insulators shall be a minimum 31 mm/kV.

#### C.6.9 STATCOM Station availability and reliability

The following definitions apply:

# C.6.9.1 Outage terms:

a) Outage

The stage in which equipment is unavailable for normal operation due to an event directly related to the equipment which results in a reduction in STATCOM Station capacity.

b) Scheduled Outage

An outage that can be scheduled at least one week in advance.

c) Forced outage

The stage in which the equipment is unavailable for normal operation but is not in the scheduled outage stage and which results in a reduction in STATCOM Station capacity i.e. an outage which is not scheduled outage.

### C.6.9.2 Capacity terms

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Maximum Continuous Capacity (Pm)

The maximum STATCOM Station capacity (MVAr) for which continuous operation under normal conditions is possible.

### C.6.9.3 Outage duration terms

Actual Outage Duration (AOD)

The time elapsed in hours between the start and end of an outage.

### C.6.9.4 Time Categories

- a) The number of hours in the reporting period in a full year, the period year is 8760 hours. If the equipment is commissioned, part way through a year, the period hours will be proportionately less than 8760 hours.
- b) Total Outage Hour (TOH)

The sum of all outage duration within the reporting period. TOH = AOD

### C.6.9.5 Availability and Reliability Terms

### Unavailability:

Unavailability is the duration for which the STATCOM Station is not available with a specified rating due to forced outages per year. If part of the station is unavailable, then the unavailability duration shall be counted proportionally. However, if STATCOM is out then its duration shall count as a fully unavailable STATCOM Station. However, If the STATCOM unit is out then the STATCOM Station unavailability shall be counted proportionally to STATCOM capacity. STATCOM Station Control system outage shall count as full STATCOM Station unavailability.

'OF' is the outage frequency which will be the number of forced outages per year.

The period basis for availability and reliability calculations shall be 12 months. The TSP shall ensure that the design will meet the specified guaranteed and design target value of availability and reliability.

Outage times for repair, maintenance and replacement of components shall be based on the premise that all items in the list of recommended spare parts are on hand, and that all maintenance schedules of recommended maintenance are adhered to. Reliability calculations shall be made and shall be presented as the expected frequency of unscheduled

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loss of STATCOM Station capacity. For simultaneous occurrence of events, for either of which a loss of capacity would result, the longer repair time shall be counted.

The facilities shall be assumed to be utilized 100% of the time at 100% load, regardless of the actual reactive power generated/absorbed by the STATCOM Station. Hence the availability and reliability assessment will be based on the capability of STATCOM Station to generate/absorb the rated reactive power regardless of whether, it is in service or not.

### C.6.9.6 Availability Requirement

The calculated availability of the system considered on an annual basis shall be equal to or exceed the following target values.

Minimum availability requirement of each complete STATCOM Station

Guaranteed for STATCOM Station - 98%

The outages of STATCOM Station capacity caused by the failure of equipment outside the scope of the TSP shall not be considered for the calculation of availability and reliability guarantee. However, such outages shall be restricted to

- 1) Complete loss to 400 kV supply (at PCC)
- 2) Human Error.

Circumstances causing curtailment of STATCOM Station capacity that will be included in reliability and availability assessment and which can lead to forced outages shall include but not be limited to the following:

- a) Failure of equipment
- b) Mal-operation of control and protection system
- c) Failure to start
- d) Reduction in capacity.

# C.6.9.7 Reliability Requirement

a) Reliability

In the assessment of reliability, the following events shall also be considered to constitute a STATCOM Station outage:

i) A STATCOM Station shut down.

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 A reduction of STATCOM Station capacity due to an outage of any component of STATCOM Station

The calculated reliability of the complete STATCOM Station shall be equal to or exceed the following design target values.

The average outage frequency per year for each STATCOM Station shall not exceed the following values:

			Design target for STATCOM	Max acceptable Guaranteed
			Station	value for STATCOM Station
Total	Number	of	3 x Nos. of STATCOM	5 x Nos. of STATCOM
Forced Outages			Station	Station

C.6.9.8 GUARANTEED FAILURE RATE OF Sub-modules. (Including all components and electronic). The maximum annual guaranteed failure rate of sub module (including all components and electronic) shall not exceed 1.0% per STATCOM. The failure rate shall not include failures directly attributable to operation and maintenance errors.

#### C.6.9.9 GUARANTEED VALUE OF FAILURE RATE OF AC POWER CAPACITOR

The maximum guaranteed annual capacitor failure rate shall not exceed 0.15% except for first unit failure. The capacitor shall be considered as failed if its Capacitance value varies more than  $\pm 5\%$  of the (actually measured) name plate value. Leakage of oil from the capacitor and the deformation of the capacitor unit shall be considered as a failure even if the capacitance value is within the tolerance limits.

### C.7 Design Principles

The objective for the design of the STATCOM Station shall be to achieve a high level of availability and reliability as specified. Special attention shall be given to designing the STATCOM Station to avoid forced outages. The TSP shall conduct thorough design reviews to ensure the minimum risk of such outages. The TSP shall give careful attention to related factors affecting STATCOM Station performance such as subsystem and system testing, protective relays co-ordination and proper setting of relays.

Except where greater reliability requirements are specified in these specifications, the design basis for STATCOM Station shall be such that no single contingency downstream from the medium voltage bus shall cause a total outage of the STATCOM Station. The following general criteria shall be followed for the design of the control system:

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- a) Use of components similar to those whose reliability has already been proved in use.
- b) Use of good design practices, surge protection, filtering, and interference buffers to assure Immunity to sensitive components and circuits against damage and interference by induced voltages and currents in the external cabling and cubicle wiring.
- c) Use of fail-safe and self-checking design features.
- d) Use of component and equipment redundancy, by means of either duplication or triplication with automatic transfer facilities wherever necessary to meet the requirement of these specifications.
- e) Design which in the event of component failures, provides for transfer to a less complex operating mode.
- f) Provision of alarm, fault diagnosis and indication

### C.8 STATCOM Station Main Components

#### C.8.1 STATCOM Unit

The main electrical data of the STATCOM Units are the following:

0	Rated voltage	20 kV Minimum

o Rated frequency 50 Hz

o Redundancy (Sub Module) 2 Nos. or 5% whichever is

higher

o Rated Power of each STATCOM unit/Branch ±50 MVAr Minimum

o Valve Cooling Deionized/Demineralized water

In general, the STATCOM units shall equally share the load however under contingency conditions it should be possible to run the units with unequal load. Charging of the DC capacitors of Sub module during the initial start-up shall be achieved by means of Resistors and bypass breaker arrangement. The charging resistor for DC capacitor of the STATCOM Sub module should be designed for three charges per hour followed by the appropriate cooling time. Power for the gate level control shall be derived internally from Sub module. The offered STATCOM Units with their Control system shall be suitably located inside the STATCOM Station Building.

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#### C.8.1.1 STATCOM Valve

The valve shall be designed to meet the performance requirements described in this specification and as described below.

In order to ensure a modern low loss and reliable solution, the STATCOM valve assembly shall use the multi-module (including redundant sub-modules) approach.

The valves shall be designed to ensure satisfactory operation according to the overall performance requirements and include all necessary auxiliary equipment required for smooth and reliable operation. The valves shall be indoor air-insulated and cooled by demineralized water. The valves shall be of modular design and have removable Sub-Module for ease of maintenance. The valves shall be mounted to allow easy access for visual inspection, routine maintenance and replacement, and facilities shall be provided to enable easy access.

#### C.8.1.2 Semiconductor Switches

The electronic switches should be designed with the aim to achieve operation according to the overall performance requirements of the STATCOM Station. The valve shall be designed with individual semiconductor switches applied in a conservative manner with regard to their basic design parameters. The semiconductor switch shall meet the requirements of IEC 60747 except where otherwise specified herein.

The semiconductor switches shall be designed to withstand all stresses expected under steady state, transient and temporary overvoltage conditions. Basic semiconductor devices shall be of the Press Pack type, or packaged to provide short circuit means in case of device failure such that the STATCOM can continue to operate without interruption. The adjacent sub-module should be protected against the possible explosion of the semiconductor switch.

Under the restriction of redundancy (minimum two or 5% whichever is higher) i.e. the failure of any semiconductor switch or sub module or monitoring device etc shall not prevent continued system operation. In the event of any of the above failures, the STATCOM shall annunciate and identify the specific location of the failed device and continue operation until such time as repairs can be scheduled. During such time the next shutdown can be availed, the STATCOM must continue to operate without downgrading STATCOM capability.

The switching device's design should include an appropriate allowance for unequal voltage distribution across individual devices in the valve due to the stray capacitor and component tolerances.

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The switching device's design should include an appropriate allowance for unequal voltage distribution across individual devices in the valve due to the stray capacitor and component tolerances.

Each switching device should be able to operate within component ratings, generally with at least two failed sub-module or levels. The number of possible failed sub-modules or levels as specified shall be consistent with the availability requirements of the STATCOM system.

### C.8.1.3 Sub module for Multi-Module Topology

The key element of the multi-module topology shall be the sub-module. By increasing the number of these sub-modules, it is possible to obtain high voltage with extremely low harmonic distortion and very low dv/dt using a low switching frequency that reduces power losses. Sub-module shall have the following characteristics:

VSC sub-modules should be protected against over voltages with appropriate strategies. A description of the failure mode of the switching device and the strategies used for failure should be provided.

In each fiber optic cable (having multiple fiber cores) used for control/communication purposes of sub-module at least two fiber cores shall remain available as spare for future use.

C.8.1.4 The STATCOM sub-module has DC capacitors that require a charge to allow full functionality and performance. At the startup of the STATCOM Station, the capacitors are discharged. During the energization sequence of the STATCOM, Capacitors are charged from the main power grid via resistor operated in series to the main connection circuits. Once the desired charging voltages are reached, the charging resistor circuit is bypassed using a bypass switch/breaker.

The Type and Rating of the charging resistor and associated bypass switch shall be designed with the aim to achieve operation according to the overall performance requirements of the STATCOM Station and shall conform to the relevant Standard.

### C.8.1.5 STATCOM Valve Cooling system

A closed-loop recirculating system shall be provided with full heat rejection capacity with redundancy for pumps, heat exchangers, and fans, appropriate to the STATCOM Station availability requirements. The cooling system should be able to maintain full capacity at maximum ambient temperature and maximum STATCOM reactive power output. The cooling system should be able to operate at the lowest ambient temperature and zero output specified. The Valve cooling system shall have black start capability and necessary

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Uninterruptible Power Supply (UPS)/ Uninterruptible Motor Drives (UMD) shall be provided separately for each STATCOM Unit.

The valve cooling system shall be designed to meet the performance requirements described in this specification and as described below.

- a) Each STATCOM Unit shall have its own de-ionized water valve cooling system with redundant pumps.
- b) For cooling the STATCOM valves, a deionized re-circulating (closed loop) water system shall be used.
- c) Water to air heat exchanger shall be used for cooling of this de-ionized water. Water to water heat exchanger shall not be employed.
- d) System shall be designed such that no shut down of STATCOM be resorted to for making up the deionized water in the system. The make-up water should comply with the recommended pH and purity.
- e) Cooling water shall have a constant flow rate irrespective of loading. The flow rate shall be decided on the basis of extreme operating conditions.
- f) The control system for the cooling system shall be redundant type including the provision of redundant control supply and main power supply. However, in place of the redundant control system for the cooling systaem, suitable alternate mode is also acceptable meeting the requirement of fulfilling cooling system operation even if failure of cooling control system.
- g) 2x100% pumps with one as standby shall be provided for the primary. In case a pump failure occur, the second pump shall automatically switch in without shutting down the STATCOM. An alarm shall be displayed at the control panel for the failure of the first pump and standby pump in operation.
- h) Each cooling system shall be provided with an independent/dedicated UMD supply however common battery for both UMD power supply may be accepted. An UMD system will provide an extended capability of the STATCOM Station to deliver reactive power without any interruption, adding a buffer against the system faults or during events such as delayed voltage recovery or Transient over Voltage (TOV).
- i) The secondary cooling system shall be a redundant type such that it shall be possible to take out 10% (minimum one number) of the cooler module (fan unit) of secondary cooling system without affecting the rated performance of STATCOM).

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- j) Normally no make-up water shall be required however in case of expansion vessel level going low; the same shall be replenished automatically by means the of make-up water tank and make up water pump to be supplied with the system.
- k) TSP shall provide a water treatment plant of sufficient capacity. The purification (treatment) system shall be designed to maintain conductivity below 1 micro Siemens. A resistivity cell in the outgoing water from the deionizer should detect the depletion of ionized material. Filters and deionizers shall be designed to allow replacement during operation. Normal replacement shall not be required more than once every year.
- I) Filters and deionizer/deoxidizer material shall be designed to allow replacement within minutes without shutdown of the cooling unit. (Normal replacement should not be required more than once/year).
- m) Primary cooling system shall monitor its own operation and condition of cooling water.
- n) The protection system of the cooling cycle shall have minimum following alarms:
  - i) Depleted deionizing cell
  - ii) Low water resistivity
  - iii) High water temperature
  - iv) Primary pump stopped
  - v) Fan stopped
  - vi) Primary pump or fan interlock circuits faulty
  - vii) Primary cycle (Make-up water) tank level low
  - viii) Failure of control supply.
  - ix) UMD/UPS fault.
- Following shutdown alarms / TRIP shall be provided with cooling system protection.
   Excessive low water resistivity Excessive high water temperature, complete loss of auxiliary supply to primary pumps, low flow, Low Pressure etc.
- p) The dissipative components of the converter are cooled with deionized water.
- q) The power losses are transferred to the external ambient by means of a deionized water /air heat exchanger. All the piping and other components shall be provided. Complete instrumentation set including following shall be mounted on board in order to check the status of the cooling system:
  - Conductivity gauge system.

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Flow meter equipped with two set points (alarm and trip).

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- Pressure meter
- Two thermometers for the inlet and two thermometers for the outlet (two set points for alarm and trip)
- Thermostat
- r) The status of the cooling system shall be monitored by means of the control system.
- s) Replacement of certain cooling equipment (e.g. pumps, fans, cooler unit etc.), if defective, shall be possible while the cooling system still operates.

#### C.8.1.6 Tests on STATCOM Unit Valve

All applicable tests i.e. Operational Type Tests, Dielectric Type Tests and Test for valve insensitivity to electromagnetic disturbance and Production tests shall be done as per the latest edition of IEC 62927.

# C.8.2 STATCOM Station Control equipment and operator interface

#### C.8.2.1 Control Equipment

The control systems should achieve the functional objectives given in 6.2. The accuracy of voltage should be within  $\pm$  1% of the reference voltage. The accuracy of the gradient and linearity of the slope delivered by the STATCOM Station should be defined in relation to the current deviation from the theoretical slope defined in 3.1. The maximum deviation should be less than  $\pm$  5% of the nominal current.

The control system design shall be based on a single fail criterion i.e. failure of any one component in the system should not result into outage of the complete system. As a minimum, a dual (hot standby) digital programmable controller shall be supplied for each STATCOM unit/branch and STATCOM Station to control the STATCOM, MSRs and MSCs completely including the functions listed as mentioned below:

- a. The controller shall have diagnostic and self-checking features for both itself and for valves, gate firing and drive circuits, interface hardware, and software. This is required to reduce outage times and to facilitate fault finding.
- b. The Controller shall be reprogrammable. The Owner shall have at least the following possibility for changing the following reference and limit values via HMI:
- c. Closed loop Controllers:

The STATCOM Station controller shall have the means to modify the reference set points. This refers to the functionality that will allow all the control parameters to be adjustable within selectable limits and is inclusive of, but not limited to following:

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- o Voltage controller
- o Q controller (reactive power controller).
- o Supplementary VSC current controller.
- o Other supplementary control functions.

### d. Sequence Controllers:

The sequence control and open-loop controllers shall include the control of all switchgears and associated control gear and external devices.

- e. The Controller shall have at least 10% excess I/O capacity to allow future program upgrades to satisfy the changing requirements of the power systems or future extensions to the STATCOM Stations. As a minimum, a control of up to 4 future HV shunt devices (reactors or capacitors) shall be included in the offer.
- f. All control signals available for remote control must also be available locally so as to ensure that a local operator can operate the STATCOM Station if the communications link between STATCOM Station and remote control centers is lost.
- g. A changeover switch shall be provided for control of the selection of local or remote control.
- h. TSP shall provide the equipment necessary for the purpose of control, protection and interlocking of all equipment within the scope of supply.
- i. TSP shall be responsible for the design and coordination of control, protection and interlocking system and switching sequences within the STATCOM Station. All necessary interfacing required between AC switchyard equipment and STATCOM Station for the above purpose shall also be included in the scope of TSP.
- j. It is proposed to control STATCOM through a Supervisory Control and Monitoring System (SCADA). All the data shall be acquired through suitable means from the field and various components and control is executed through the redundant HMI. The local STATCOM Station Control system shall consist of a redundant STATCOM Station controller, redundant HMI workstation, Gateway, STATCOM Station Control System Engineering cum Disturbance Recorder (DR), PC which can also be used as standby HMI workstations in case of emergency with associated peripheral equipment such as color laser log Printers, Color laser jet fault record printer, GPS System, Inverter / UPS etc. all interconnected via redundant Ethernet based Station LAN Network. Each work-stations and PCs at STATCOM Station shall have at least 19" LED display.
- k. In addition to the above, HMI workstation (identical to HMI Workstation provided in the STATCOM Station control room) should also be provided in the control room of the main

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400kV substation. This HMI workstation should be powered from an independent UPS system adequate enough to provide power to the HMI workstation for a minimum two hours in case of auxiliary power failure.

- I. The control equipment shall satisfy the reliability and availability requirements specified in this specification
- m. All necessary measures shall be taken to ensure satisfactory operation in the presence of harmonic current and voltage, noise and radio interference signals. The equipment shall be designed to operate in the environmental conditions specified in the specification.
- n. There should be a provision for independent operation of MSC/MSR after delinking it with STATCOM controls when STATCOM is out of service due to any reason.
- o. The threshold values for switching the MSC/MSR on/off shall be configurable in all modes of operation.

### C.8.2.2 Operator Interface

- a) Each STATCOM Station shall have a SCADA consisting of an HMI which shall provide a Centralized (local) operator control of the STATCOM Station functions. All human interface operations necessary for the control and monitoring of the STATCOM shall be provided at this point.
- b) Any abnormal condition requiring operator action or intervention or maintenance on any of the STATCOM Station subsystems shall be annunciated at the STATCOM Station control room and the Substation control room.
- c) The local HMI shall include the following diagrams as different screens in the display system:
- Complete STATCOM Units and STATCOM Station single line diagram including EHV and MV busses
- ii. AC Auxiliary supply and distribution
- iii. DC Auxiliary supply and distribution
- iv. STATCOM Valve cooling systems
- v. Interlocking system.
- d) These diagrams shall indicate status, alarms, voltages, currents, etc. The HMI shall provide complete diagnostics on alarm and trip indications as required and discussed in this specification, including SER information.

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- e) A facility shall be provided whereby the local HMI features and functions shall be accessible from remote. A remote user shall be able to view screens and change STATCOM Station parameter settings.
- f) As the substation where STATCOM Station shall be installed, will be equipped with Substation Automation System (SAS) conforming to IEC 61350, it is required that STATCOM Station control and monitoring shall be integrated with SAS at the main Sub-station by the TSP. It is proposed to connect STATCOM Station's SCADA with SAS through a Gateway and the database, configuration etc of the main substation SAS shall be upgraded to incorporate STATCOM Station events, alarms, Controls (both switchgear and control functions of STATCOM Station like the setting of parameters etc.) so that STATCOM Station can be effectively monitored and controlled from main substation SAS and shall be monitored from Load Dispatch Center (RLDC).

### C.8.3 STATCOM Station Protection System

### C.8.3.1 Protection system Design

- a) To ensure that faults are cleared within stability critical clearing time, to minimize damage to the plant, and to avoid voltage collapse, loss of load, or load limitations, TSP shall provide a high speed main protection scheme. An independent (having a separate measurement system) back-up protection scheme shall be provided in the event of the main protection scheme failing or taken out for maintenance.
- b) The STATCOM Station shall be completely self-protecting (unit protection). STATCOM Station shall be protected from damage for all conditions of over-current, overvoltage, excessive reactive power loading, unbalance due to loss of capacitor elements, phase-to-phase and phase-to-ground faults, three phase faults, loss of cooling, semiconductor valve or control malfunction, faults (STATCOM, MV system) in individual primary connected components of the STATCOM, HV system faults, etc. The STATCOM Station shall withstand the maximum fault current for a period of the maximum fault clearing time as specified, considering second contingency cases due to the previously mentioned conditions.
- c) All protection equipment and systems should be properly co-ordinated to prevent incorrect operations of the protection equipment or systems during normal STATCOM Station operation, including anticipated abnormal conditions on the transmission system, as specified. Fail-safe principles should be applied throughout.

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- **C.8.3.2** The basic principle and order of precedence for the control and protection shall be, to take care of the following:
  - Correctly identify a fault, problem or error condition,
  - Only if necessary, isolate the minimum number of components, subsystems whenever possible,
  - Utilize degraded modes to the maximum extent possible either directly (no
    interruption of the STATCOM Station operation) or indirectly (by tripping the
    STATCOM Station momentarily in order to isolate the branch and re-energization of
    the STATCOM Station).
  - Trip STATCOM Station and Block.
    - a) Failure of the STATCOM Station Interface (SCADA interface) shall not result in a Protection trip of the STATCOM Station. A fail-safe philosophy shall be implemented to allow the STATCOM Station to operate safely and independently from the STATCOM Station Interface (SCADA interface).
    - b) Protection equipment shall be designed and applied to provide maximum discrimination between faulty and healthy circuits.
    - c) The Protection shall be sufficiently sensitive to cater to the full range from maximum to minimum fault level conditions. The Protection shall also be suitable for a system fault level equal to the maximum short circuit capacity of the substation. All current transformer designs shall be based on these fault levels.
    - d) All required protective, control devices, etc including auxiliary instrument transformers and panels, relays, cabling, wiring, indication, and all other associated plant and material necessary for the effective operation of the protection systems shall be supplied and installed by TSP.
    - e) The protective relays shall be microprocessor based. Relays shall have approved characteristics and be mounted in dust and moisture-proof cases. The protective relays shall be provided with visual indications for starting, tripping and failure of the protective function. The LEDs shall be reset without opening the covers. The protection relays shall also be equipped with HMI facilities suitable for manual parameter settings and viewing of the settings. Relays with provision for manual operation from outside the case, other than for resetting, are not acceptable. Relay settings shall be visible and readable without having to remove the relay cover. Relays shall be of approved construction and shall be arranged so that adjustments, testing and replacement can be effected with the minimum of time and labor. Auxiliary Relays of the hand reset type, if provided shall be capable of

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being reset without opening the case. Electrically reset tripping relays shall be provided as necessitated by the system of control, such as for those circuits subject to remote supervisory control.

- f) Relay contacts shall be suitable for making and breaking the maximum currents which, they may be required to control in normal service but where contacts of the protective relays are unable to deal directly with the tripping currents, approved Auxiliary tripping relays shall be provided. In such cases, the number of auxiliary tripping relays operating in tandem shall be kept to a minimum in order to achieve fast and reliable fault clearance times. Separate contacts shall be provided for alarm and tripping functions. Relay contacts shall make firmly without bounce and the whole of the relay mechanisms shall be as far as possible unaffected by vibration or external magnetic fields
- g) Steps shall be taken to protect the circuitry from externally impressed transient voltages which could reach the circuitry via connections to instrument transformers or the station battery. The routing of cables should be such as to limit interference to a minimum. Any auxiliary supplies necessary to power solid-state circuits shall be derived from the main station battery and not from batteries internal to the protection.

### h) Relay communication

The Relays shall also have a communication port provided on the front of the relay for configuration and parameter settings as well as downloading of data. A direct port suitable for remote communication shall also be provided at the back of the Relay. This port shall conform to IEC - 61850.

### i) Tripping schemes

- Tripping of MV circuit breakers shall be done by means of two-separated trip signals.
- Duplicate high security tripping circuits for MV Circuit Breaker shall comprise two independent high speed (less than 10 ms) high burden (greater than 150 W) tripping relays for each circuit, each with its own independent DC supply. The trip circuits for all circuit breakers need to be equipped with a "lockout" function and it shall be possible for this to be reset manually and remotely by the operator.
- j) The protection for the power system is based on a normal switching state and an occurrence of a single fault. This means that faults resulting from maintenance as well as the simultaneous occurrence of two or more faults are not taken into account.

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k) The input circuits of the digital protections shall be monitored by means of a plausibility check. If any incorrect information is found, the protection function shall be blocked by the protection system. All protection relays shall have facilities for monitoring trip circuits. Detection of an interruption in the case of a switched on circuit breaker shall be signaled.

### 1) Test facilities

- It shall be possible to test the protective device during operation without causing trips. Links shall be provided for the isolation of individual protection trip circuits and the common protection trip circuit to each circuit breaker trip coil.
- Separate test facilities shall be provided for each current and voltage transformer secondary circuit so as to give access for testing of protection relays and associated circuits. The Test facility to be supplied shall have two selectable positions, a Service and a Test position. In the service Position, the test switch connects CTs and VTs signals to the Relays and trip commands to the circuit breaker trip coils. In the Test Position, the test switch applies a short-circuit to the Current Transformer (CT) secondary windings and open circuits the VT secondary cores and allow injection of secondary current and voltage into the relay. At the same time, the Trip commands to the Circuit Breaker Trip Coils are isolated. The test switch supplied shall be to the Approval of the Owner.
- m) The protection of the electrical system shall be designed and installed in such a way that the failed equipment is disconnected selectively and automatically. All equipment have to remain operative during transient phenomena, which may arise during switching or other disturbances to the system.

# n) Auxiliary DC Supplies

The protection concept has to be designed in a way so that back-up protection is provided at all times. All protection relays shall be configured in a way that failure of one Auxiliary DC system will not affect the relay. If all DC supplies to the controllers are lost, the STATCOM Station breaker must be tripped via the protection panel.

### o) Electromagnetic Compatibility

- Electronic Relays and other electronic devices and the ancillary circuits connected to them, such as power supplies, current and voltage transformer secondaries, status or tripping or alarm circuits shall be designed to ensure that they are compatible for use in the hostile electrical environment found in an MV or HV substation.
- Adequate steps by means of suitable design, shall be taken to prevent Electromagnetic Interference (EMI), (generated by sources such as circuit

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- breakers, disconnectors, lightning, radio or radar emissions, switching contactors in DC circuits etc) or Electrostatic Discharges (ESD) from affecting relay performance or causing damage to components.
- All relays offered shall therefore have been type-tested to meet the current requirements of IEC Standards with respect to High Frequency disturbance, Fast Transients, Electrostatic Discharge, Radio Frequency Interference testing etc.
- p) List of Protection functions for STATCOM Station

### **Coupling Transformer Protection:**

- i) Biased Differential Protection (87T)
- ii) REF Protection (64T)
- iii) OverCurrent Protection (50, 51)
- iv) Ground Over Current (51N)
- v) Over Flux Protection (HV and MV)
- vi) Transformer Mechanical Trips

#### **STATCOM MV Bus Protection:**

- i) Bus Differential Protection (87)
- ii) Ground Over Current Protection (51N), used with a neutral Grounding Transformer
- iii) Under / Over Voltage (59 Ph-Ph) Protection
- iv) Over Voltage (Open Delta) Protection

### **STATCOM Branch Protection:**

- i) Differential Protection (87)
- ii) Overload Protection (49)
- iii) OverCurrent Protection inside delta (50, 51)
- iv) Negative phase sequence protection (46)
- v) STATCOM branch overcurrent protection (50, 51, 50N, 51N)

# **MSR Branch Protection:**

- i) Differential Protection (87)
- ii) Ground Over Current protection (51N)
- iii) Reactor branch unbalance protection (Negative Phase Sequence)
- iv) Thermal Overload protection

## **MSC Branch Protection:**

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- i) Ground Over Current Protection (51N)
- ii) Capacitor OverVoltage (Using current signal) protection.
- iii) Capacitor unbalance protection (60C)
- iv) Over Current Protection (50, 51)
- The protection functions listed above are the minimum set of function to be provided, any additional protection required to fulfill the requirement of the protection system shall also be provided.
- Further protection functions of individual branch (STATCOM, MSC, MSR) shall trip the respective branch MV CB (Circuit Breaker).
- All CBs shall be provided with individual Breaker Failure protection relays. Breaker Failure relay shall have the logic based on the current signal or CB close open status.
- Any fault on MV bus will trip the 400 kV breaker. However, any branch fault shall be cleared by the respective MV branch Circuit Breaker.
- Protection System for the STATCOM valve portion of the STATCOM station shall be provided in the redundant controllers to isolate the STACOM valve during internal overload/overvoltage, ground fault etc.

### C.8.4 STATCOM Station Fault Recording System

An integrated Transient Fault Recording (TFR) System shall be supplied, installed and commissioned. This shall include trigger level settings for analog signal, etc subject to review and comment. Disturbance and event recording facilities are required for local monitoring of the STATCOM following a disturbance on the power system or the STATCOM System. The TFR shall be GPS synchronized.

The following inputs are required:

- All analog signals (output signals) including 3-ph and sequence values of voltage, control.
- All digital signals (control outputs, status indications, commands, alarms, and trip indications). Internal STATCOM Station control signals/variables to be selectable.
- The accuracy of the TFR for event inputs shall be at least 100 μs (sampling rate of minimum 10 kHz).
- The TFR shall have provision for remote access and retrieval of recorded information onto a PC. For this purpose, a communication link to the substation LAN shall be implemented.
- The remote software application for data retrieval shall be included.
- There shall be multiple channels to view 3-ph and sequence values of voltage,

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current.

TFR file shall be viewable in any open source software.

### C.8.5 Mechanically Switched Reactor (MSR)

MSR is a fixed source of inductive reactive power connected in shunt to the MV bus of STATCOM Station and switched by means of a circuit breaker (with a control switching device) based on the command from the STATCOM Station control system. The rated capability of MSRs shall be at 400kV (Referred to as "Point of Common Coupling" or PCC) and in the steady state frequency range of 48.5 Hz-50.5 Hz. However, the MSR Components shall be designed with the aim to achieve operation according to the overall performance requirements of the STATCOM Station. The individual components of MSR shall be able to withstand the onerous conditions imposed by system overvoltage and harmonics. The MSR consists of 3-ph Air Core Reactor, 3-ph MV Circuit breaker (SF6/Vacuum type), associated current transformer, 3-ph Disconnector and associated safety grounding switch. The MSR area shall be fenced and a castle key interlock with safety grounding switch shall be provided for human safety.

Specifications for individual components like Air core reactors etc are provided in the subsequent clause.

#### C.8.6 Mechanically switched capacitor (MSC)

MSC is a switched 3-phase capacitor bank connected in shunt to the MV bus of STATCOM station and switched automatically by means of a circuit breaker (with control switching device) based on the command from STATCOM Station control system. The rated capability of MSCs shall be at 400 kV (Referred to as "Point of Common Coupling" or PCC) and in the steady state frequency range of 48.5 Hz-50.5 Hz. However, TSP will ensure the corresponding values at PCC (400 kV) for possible operating condition measured at PCC. The MSC Components shall be designed with the aim to achieve operation according to the overall performance requirements of the STATCOM Station. The individual components of MSC shall be able to withstand the onerous conditions imposed by system over voltages and harmonics. The MSC consists of 3-ph AC power capacitor bank, a current limiting air core reactor as required, 3-ph MV Circuit breaker (SF6/Vacuum type), associated current transformer, 3-ph Disconnector and associated safety grounding switch. The MSC area shall be fenced and a castle key interlock with safety grounding switch shall be provided for human safety. Specifications for individual components like Capacitors, Air core reactors etc are provided in the subsequent clauses.

### C.8.7 Air Core Reactors

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- a) Reactors shall be air core, dry type, be suitable for outdoor installation and there shall be no tapping on the reactors. The insulation level shall be adequate and TSP has to ensure proper insulation coordination.
- b) The insulation of the reactor shall be class F and hot spot temperature rise shall not exceed 105 °C above ambient temperature. Winding temperature rise shall not exceed 80 °C above ambient temperature.
- c) The reactor shall be designed to withstand thermal dynamic shocks and mechanical shocks while in service and during erection.
- d) The reactor shall fully conform to the relevant IEC standard.
- e) The reactor shall be designed to withstand overloading due to over voltage as specified and shall also be subjected to excitation by harmonics; the reactor must be able to withstand such events without deterioration in normal life.
- f) The reactors shall be subjected to type and routine tests in accordance with the latest issue of IEC-60076 as appropriate to the type of reactor provided.
- g) Tests on Reactors: The reactors shall be subjected to type and routine tests in accordance with the latest issue of IEC-60076 as appropriate to the type of reactor provided.

#### C.8.8 AC POWER CAPACITORS

- i) General
- The capacitor banks shall comprise capacitor units, discharge devices, protection equipment, series reactor as required, earthing switches, suitably connected in series and parallel, mounted at ground level with protected fencing all around. The number, arrangement and connection of capacitor banks shall be designed to suit the requirement of the compensator as a whole. If convenient, the capacitor banks may be used in conjunction with reactors. In this event, the rating of the capacitor shall be adequate to cope up with the harmonic loading. The frequency variations shall also be considered. To limit the peak inrush current for switching in the capacitors, current limiting reactors with parallel connected damping resistors, if required shall be connected in series with shunt capacitor banks.
- b) The capacitors shall be provided with internal-type fuses. Alternatively, the fuseless capacitor is also acceptable.
- c) Fuses shall not melt nor shall deteriorate when subjected to the inrush current during the life of the capacitor bank.

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- d) With the capacitor charged to a peak voltage, the fuses associated with the healthy elements shall not melt when carrying the discharge current resulting from a breakdown of an element or from an external short circuit.
- e) Fuses shall be capable of disconnecting a faulty element over a range of voltage across the unit terminals from 0.9 U<sub>n</sub> to 2.0 Un. In addition, if all the elements in the same row of an internally fused capacitor were to fail as a result of a cascading action, the last fuse element to melt shall be capable of successful disconnection with a voltage of not less than 1.5 times.
- f) After fuse operation the fuse assembly shall be able to withstand continuously at least 1.5 times the rated unit voltage  $U_n$  across the gap for 10 Seconds.
- g) Fuses shall preferably be of the current limiting type but fuse system shall in any event be designed to ensure that energy released into a faulty capacitor unit is less than the valve that will cause rupture or bursting of the container.
- h) The capacitor units shall be the outdoor type. The container of the capacitor shall be of stainless steel.
- i) Each capacitor unit shall be readily accessible and replaceable without disturbing any other unit. The supporting frames shall be designed to provide adequate ventilation to the units.
- j) The dielectric fluid used in the capacitor unit shall be environmentally safe and biodegradable, non-toxic. Polychlorinated bi-phenyl (PCB) type dielectric or any of its derivatives shall not be acceptable.
- ii) Construction and Design Requirement
- a) The capacitors shall conform to IEC-60871. The capacitors shall be provided with internally mounted discharge resisters with characteristics in accordance with IEC-60871.
- b) The current limiting reactors (as required) shall be dry type and connected in series with the capacitor bank. Suitable lifting lugs shall be provided.
- c) The capacitor enclosure shall have sufficient strength to withstand without damage or loss of life, mechanical load, both in operation and during erection. The loads shall include electromagnetic forces including those during faults external or internal to the capacitor bank, wind loading, forces due to expansion and contraction caused by ambient temperature and load variation, and seismic effects all as specified.
- d) The capacitor units shall be interchangeable in order to reduce the spare requirements and simplify maintenance procedures.
- e) The capacitor stack shall be vibration free. The stack shall have a fixed potential that is connected to one electrical point in the bank. The stack shall be of galvanized structural steel.

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- The capacitor racks shall be supplied complete with all capacitor units, insulators, and connections and shall be equipped with lifting lugs/eyes to facilitate assembly into the stacks. The racks shall be constructed of galvanized structural steel. No drilling of galvanized steel shall be allowed. Each rack shall be labeled with the weight of the fully equipped racks, the phase, and the bank of which it forms a part. The maximum and minimum capacitor unit capacitance which may be substituted into the racks as spares shall be suitably identified. Suitable warning labels shall be affixed.
- g) The capacitor shall be specially designed to be suitable for intermittent duty.
- h) The capacitors should comply with the overload capacity as per NEMA Standard.
- i) The capacitor elements shall be vacuum dried inside the case prior to impregnation with dielectric fluid. After impregnation, the capacitor unit shall be sealed immediately upon removal of the impregnated reservoir.
- j) The discharge resister shall discharge the unit from peak operating voltage to less than 75 Volts within 10 minutes.
- k) The capacitor case shall be made from type 409 stainless steel or equivalent stainless steel with all joints welded and tested for leaks.
- All racks and bus insulators as well as the insulators used to insulate each stack of capacitor from ground level shall be pin cap or post type. The minimum voltage rating shall be 15 kV and low frequency wet withstand voltage of all insulators used to insulate within or between the capacitor rack of a stack shall not be less than three times the actual voltage stress across the insulators. The insulator shall be outdoor type manufactured from wet porcelain. The insulators shall be bolted to the top members of the frame to support electric-grade aluminum buses.
- m) The size and groupings of the individual capacitor units shall be such that a single blown fuse will not cause the voltage across the parallel group to rise by more than 10%.
- n) The redundancy to be provided, shall be as per the requirement specified regarding reliability and availability in the clause mentioned elsewhere.

### iii) Capacitor Unit Failure Detection

The stages of capacitor units or element failure detection shall be provided as below:

a) A three-step unbalanced current protection shall be provided in each capacitor bank to initially generate an alarm when the unbalance limit is reached and finally to trip the bank in case of the limit is exceeded.

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- b) The first stage shall generate an alarm and the capacitor unit shall continue in service. It may be assumed that the bank shall be disconnected for maintenance within 2 weeks.
- c) The second stage shall generate a separate alarm and a delayed trip signal which will disconnect the bank after two hours.
- d) The third stage shall cause immediate disconnection of the Capacitor Bank.

### iv) Tests on Capacitors

All the tests on capacitor units shall be in accordance with the latest issue of IEC 60871.

#### C.8.9 Coupling Transformer

The TSP shall provide single phase coupling transformers to operate as 3- phase bank with one unit as a common spare (cold spare) with necessary auxiliary arrangements for stepping down the voltage from 400 kV system to a suitable medium voltage value as required for replacing any one of the faulty phase units without physically shifting the transformer. The Medium Voltage side of the coupling transformer to couple with the STATCOM shall not be less than 20 kV to ensure optimum power transformation.

The Coupling Transformer shall be designed with the aim to achieve operation according to the overall performance requirements of the STATCOM Station. The transformer should be designed and rated to carry complete capacitive and inductive reactive loading as specified for STATCOM Station including that of mechanically switched capacitors and Reactors etc.), as well as harmonic currents associated with the most onerous operating conditions of STATCOM Station, without loss of life.

The coupling transformer shall be designed in accordance with the most up-to-date experience in STATCOM application and shall incorporate the latest improvements of design currently employed in the industry. The Comprehensive design review of the Coupling Transformer of STATCOM Station shall be carried out by the TSP.

#### C.8.9.1 General Requirements

The coupling transformer shall be designed electrically and mechanically for operating conditions peculiar to STATCOM Station operation, which shall include, but not be limited to the following:

 Electrical insulation problems resulting from the transformer being subjected to voltages of distorted sinusoidal wave shape because of saturation, harmonics, trapped charges in capacitors etc.

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- b) The cumulative effect of electro-dynamic forces produced during valve commutation or other short circuit conditions imposed by valve design limitation and valve group operation.
- c) Harmonic currents due to STATCOM operation, with reference to additional stray losses resulting from these harmonic currents.
- d) No generation of uncharacteristic harmonics by the transformers.
- e) Stresses due to normal control operation and other onerous operations such as blocking and de-blocking.
- f) Stress due to the fast response requirement of STATCOM for loading from 100% inductive to 100% capacitive and vice-versa.
- g) Overvoltage stresses for which STATCOM shall be designed as per specification would apply to the transformer also.
- h) All other stresses for which STATCOM Station shall be designed as per specification would apply to the transformer also.
- The transformer and all its accessories like Bushings, CTs etc shall be designed to withstand without damage, the thermal and mechanical effects of any external short circuit to earth and of a short circuit across the terminals of any winding for a period of 3 seconds. The short circuit level of the 400 kV system to which the transformer shall be connected, will be as per the maximum short circuit level of the main substation. Short Circuit level of the Coupling Transformer shall be as per the Short Circuit level of the respective Substation. Short circuit level for HV bushing shall be 63 kA for 1 Sec.
- j) The transformer shall be capable of being loaded in accordance with IEC 60076 or the overload conditions as specified whichever is the worst. There shall be no limitation imposed by bushings during its terminal fault.
- k) The transformer shall be capable of withstanding the mechanical stresses caused by symmetrical or asymmetrical faults on any winding.
- The transformer should be designed to carry a certain level of direct current consistent with the STATCOM design. To ensure minimum harmonics generation, the saturation flux density of the transformer should be higher than the maximum flux density reached over the full steady state (continuous operating) range; this margin shall be at least 10%. This maximum flux density (over the full steady-state range) is obtained at the highest secondary voltage during any reactive power generation, highest reference voltage, minimum slope, and minimum continuous frequency. The flux density at the highest secondary voltage shall lie in the linear portion of the BH curve of the core. Any harmonic generated by the transformer should be considered for the design of the STATCOM.

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- m) All protection class Current Transformers in the coupling transformer shall be of PX/PS type. Other details of these Current Transformers shall be as per protection/metering requirements and shall be decided during detailed engineering. However, the parameters of the Winding Temperature Indicator (WTI) of Current Transformer for each winding shall be as per the Coupling Transformer manufacturer.
- n) Transformers shall be capable of operating under natural cooled conditions up to the specified load. The forced cooling equipment shall come into operation by pre-set contacts of winding temperature indicator and the transformer shall operate as a forced cooling unit initially as Oil Natural Air Forced (ONAF) up to a specified load and then as Oil Forced Air Forced (OFAF). Cooling shall be so designed that during total failure of power supply to cooling fans and oil pumps, the transformer shall be able to operate at full load for at least ten (10) minutes without the calculated winding hot spot temperature exceeding 140 degree Celcius. Transformers fitted with two coolers, each capable of dissipating 50 percent of the heat due to losses at the continuous maximum rating, shall be capable of operating for 20 minutes in the event of failure of the oil circulating pump or blowers associated with one cooler without the calculated winding hot spot temperature exceeding 140°(degree) Celcius at continuous maximum rating.
- o) The transformer shall be free from any electrostatic charging tendency (ECT) under all operating conditions when all oil circulation systems are in operation. In general, the oil flow speed shall not exceed 1.0 m/sec within winding in the oil flow system of the transformers. The manufacturer shall ensure that there is no electrostatic charging tendency in the design.

The Technical Parameters of the Transformer shall be as below

Si. No.	Description	Unit	Technical Parameters
1.1	Rated Capacity		
	HV	MVA	To meet the performance
	MV	MVA	requirement and ratings of STATCOM. The transformer shall be suitable for 100% reactive loading
1.2	Voltage ratio (Line to Line)		400 / XX (*)
1.3	Single / Three Phase Design		Single phase
1.4	Applicable Standard		IEC 60076
1.5	Rated Frequency	Hz	50

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Sl. No.	Description	Unit	Technical Parameters
1.6	Cooling and Percentage Rating		ONAN/ONAF/(OFAF or
	at different coolings		ODAF): 60% / 80%/100%
			OR
			ONAN/ONAF1/ONAF2: 60%
			/80%/100%
			OR
			OFAF (with 5 x 25% unit coole
			if required)
1.7	Impedance at 75 °C (in		!
	percentage)		
	HV-MV	7111	To suit the design
			requirements.
1.8	Tolerance on Impedance (HV-	%	As per IEC
	MV)		1
1.9	Service		Outdoor
1.10	Duty		Continuous Reactive loading
1.11	Overload Capacity		IEC-60076-7
1.12	Temperature rise over 50 °C	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	ambient Temp		
i)	Top oil measured by	οС	50
	thermometer		
ii)	Average winding measured by	°C	55
	resistance Method		
1.13	Windings		
i)	System Fault level		
	HV	kA	63
	MV	kA	To suit the design
			requirements.
ii)	Lightning Impulse withstand		
	Voltage		
	HV	k∨p	1300
	MV	k∨p	*
	Neutral	k∨p	170
iii)	Switching Impulse withstand		The second secon
	Voltage		
	HV	k∨p	1050

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SI. No.	Description	Unit	Technical Parameters
iv)	One Minute Power Frequency		
	withstand Voltage		
	HV	kVrms	570
	MV	kVrms	*
	Neutral	kVrms	70
v)	Neutral Grounding		Solidly grounded
vi)	Insulation		, , , , , , , , , , , , , , , , , , , ,
	HV		Graded
	MV		Uniform
vii)	Tan delta of winding	%	< 0.5
1.14	Vector Group (3 – ph)		YNd*
1	(unless specified differently		
	elsewhere)		
1.15	Tap Changer		Not Applicable
1.16	Bushing		
i)	Rated voltage		
	HV	kV	420
	MV	kV	*
	Neutral	kV	36
ii)	Rated current (Min.)		
	HV	Α	*
	MV	Α	*
	Neutral	Α	*
iii)	Lightning Impulse withstand		
	Voltage		
	HV	kVp	1425
	MV	kVp	*
	Neutral	kVp	170
iv)	Switching Impulse withstand		
	Voltage		
	HV	kVp	1050
v)	One Minute Power Frequency		
	withstand		
	Voltage		
	HV	kVrms	695
	MV	kVrms	*

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SI. No.	Description	Unit	Technical Parameters
	Neutral	kVrms	77
vi)	Minimum total creepage		Manager (g) and de
	distances	:	
	HV	mm/kV	31
	MV	mm/kV	31
	Neutral	mm/kV	31
vii)	Tan delta of bushings		
	HV	%	Refer Note 2
	MV	%	Refer Note 2
viii)	Max Partial discharge level at		
	Um		
	HV	pC	10
	MV	pC	10
	Neutral		-
1.17	Max Partial discharge level at	pC	100
	1.58 * Ur /v3		
1.18	Max Noise level at rated	dB	80
	voltage and at principal tap at		
	no load and all cooling Active		
1.19	Maximum Permissible Losses		
	of		
	Transformers		
i)	Max. No Load Loss at rated	kW	To suit the design
	voltage and Frequency		requirements.
ii)	Max. Load Loss at maximum	kW	To suit the design
	continuous current and at 75°		requirements.
	С		
iii)	Max. Auxiliary Loss at rated	kW	To suit the design
	voltage and Frequency		requirements.

# Notes:

- 1. No external or internal Transformers / Reactors are to be used to achieve the specified HV/MV impedances.
- 2. The criteria for Transformer losses shall be "Copper Loss (Load Loss) > Iron Loss (No Load Loss) > Cooler Loss (Auxiliary Loss)".
- 3. (\*) marked parameters shall be decided based on STATCOM manufacturer's requirement.

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### C.8.10 STATCOM Station MV Switchgear

The MV Switchgear shall be designed with the aim to achieve operation according to the overall performance requirements of the STATCOM Station.

#### C.8.10.1 MV Circuit Breaker

The MV Circuit Breaker shall comply with the relevant IEC standard and all other relevant Standards, and as specified in this specification. They shall satisfy the General Technical Requirements and shall be designed to operate in the environmental conditions specified in this specification.

The Circuit Breaker offered should be of SF6 type/Vacuum type only and of class C2, M2 as per IEC

- i) The circuit breaker shall be complete with terminal connectors, operating mechanism, control cabinets, piping, inter pole cable, cable accessories like glands, terminal blocks, marking ferrules, lugs, pressure gauges, density monitors (with graduated scale), galvanised support structure for CB and control cabinets, their foundation bolts and all other circuit breaker accessories required for carrying out all the functions the CB is required to perform.
- ii) All necessary parts to provide a complete and operable circuit breaker installation such as main equipment, terminals, control parts, connectors and other devices whether specifically called for herein or not shall be provided.
- iii) The support structure of the circuit breaker shall be hot dip galvanized. Exposed hardware items shall be hot dip galvanized or Electro-galvanized.
- iv) MV Circuit Breaker shall be equipped with controlled switching with consequent optimization of switching behavior, when used in:
  - Switching of Capacitor Bank
  - Switching of shunt Reactor Bank
- v) Reactor Switching Duty test shall be conducted on MV Circuit Breaker in line with latest edition of IEC 62271-110.
- vi) Type Tested for Back-to-Back Capacitor Bank Switching as per latest edition of IEC 62271-100.
- vii) Routine tests as per IEC: 62271-100 shall be performed on all circuit breakers.
- viii) The medium voltage circuit breakers in any of the branches shall be designed to switch off metallic three phase short circuits only limited by the transformer impedance of the STATCOM System (Coupling transformer) with the initial short circuit current and DC component according to IEC 60909-0. Thereby the worst case time constant where the

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maximum short circuit peak and DC component occur shall be considered. The network shall be considered to deliver the maximum short circuit power of the substation.

#### C.8.10.2 MV Isolator and Earth Switch

The isolators and earth switches shall comply with the IEC and all other relevant Standards, and as specified in this specification. They shall satisfy the General Technical Requirements and shall be designed to operate in the environmental conditions specified in this specification.

- The isolators and accessories shall conform in general to IEC-62271 series as per relevance (or IS:9921) except to the extent explicitly modified in specification.
- ii) Earth switches shall be provided on isolators wherever called for.
- iii) Switches shall be motor operated with local and remote operation features and local manual operation features. Remote operation of Earth Switch is not required.
- iv) Disconnections and earth switches shall electrically and mechanically be interlocked. Castle Key interlocking facilities shall be provided to mechanically interlock the earth switch and Isolator to the doors of valve rooms.

#### C.8.10.3 Instrument Transformers for STATCOM Station

The instrument transformers shall comply with the relevant IEC Standards. They shall satisfy the general Technical Requirement specified in the specification and shall be designed to operate in the environmental conditions specified in this Specification. The instrument transformers provided for control, metering and protective relaying functions shall have voltage and current ratings, accuracy ratings and burden capabilities adequate to provide their designated functions within the overall accuracy requirement of the systems.

### **Voltage Transformers**

Voltage transformers shall comply with the relevant IEC standards IEC 61869 (Part-1, Part-3 and Part-5).

#### **Current Transformers**

Current transformers shall comply with IEC 61869 (Part-1 and Part-2). Type tests and routine tests as per relevant IEC.

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### C.8.10.4 Surge Arrester

TSP shall install the surge arresters necessary for the protection of the equipment associated with the STATCOM Station in accordance with the requirements as per the insulation coordination study. The surge arresters shall give consistent protection to their associated equipment against overvoltage produced by lightning or switching surges, internal or external station faults, and other system disturbances.

The surge arresters shall be rated such that they are able to discharge a specified maximum energy due to the application of lightning, switching surges, temporary over voltages and faults as determined by insulation coordination studies, without coming into the temperature region where thermal runaway could result upon subsequent application of maximum transient and steady state voltage conditions.

The arrester housing shall be porcelain/composite type. The end fittings shall be made of non-magnetic and corrosion proof material.

Internal components shall be designed to eliminate internal corona and also to ensure minimal capacitive coupling with any conducting layer of pollutant on the outside of the porcelain housing. Particular attention shall be given to the high discharge currents which some of the arresters may experience in service due to discharge of stored energy of the AC filter and reactive compensating equipment, tripping of STATCOM etc.

### C.8.11 STATCOM Station Auxiliary Power Supply

The auxiliary supply of STATCOM Station shall conform with the system requirements relating to reliability, availability, and redundancy, performing continuously to help ensure that the complete STATCOM Station operates as per the requirements. STATCOM station Auxiliary supply including all necessary switchgear (viz. AC/DC, lighting boards etc.) shall be completely separate from the main 765/400/220 kV substation auxiliary supply, all loads of STATCOM station shall be fed from this supply. The auxiliary supply provides power to the controllers, cooling system, station supplies, and various other essential and non-essential loads. With the exception of the cooling system, all other essential loads are also connected to the DC system of the STATCOM Station which is also to be provided separately from the DC system of the main 765/400/220 kV substation.

The auxiliary supply system shall be able to provide a stable supply for the STATCOM Station during system faults such as single-phase faults, phase-to-phase faults, and three-phase

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faults and LVRT (Low Voltage Ride Through) to allow continuous operation of the STATCOM Station during these transient events.

The auxiliary supply system of each STATCOM Station shall consist of two main incomers and one emergency incomer from DG set. The two main incomers shall be required to be paired to act redundantly to help ensure a certain degree of reliability and availability. One of the main incomers shall be supplied from 33 kV tertiary winding of 765/400/33 kV or 400/220/33 kV ICT at the main substation.

The other main incomer can be supplied from any one of the following three options:

- Supplied from Tertiary/Yoke winding of STATCOM coupling Transformer.
- Supplied from MV Bus Bar of STATCOM Station.
- Supplied from Power PT on HV side of coupling Transformer.

Wherever the Voltage variation on the incomer is very high, a solid state AVR (Automatic Voltage Regulator) shall be provided to control the auxiliary supply voltage.

All MV incomers shall be provided with suitable CB, disconnector, instrument Transformer etc along with necessary protection system.

### C.8.12 Fire Protection System for STATCOM Station:

Necessary fire protection for STATCOM units, Coupling Transformer, MSC, MCR and Harmonic filter (if any) shall be required. The main features of these protections are as under.

#### Fire Detection and Alarm System:

Suitable fire detection system using smoke detectors and/or heat detectors shall be provided in STATCOM Station for all room and areas. These smoke fire detection systems shall be connected to a separate Fire annunciation system clearly identifying the zone.

### **Hydrant System:**

The hydrant system shall be extended from fire fighting system of the substation in the yard. Suitable number of hydrants shall be provided for protection of STATCOM Station equipment in the yard namely Coupling Transformer, MSCs, MSRs and Harmonic Filter (if required) etc as applicable for the station. Further suitable number of hydrants shall also be provided for STATCOM Station building

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#### **HVW System:**

HVW (High Velocity Water) Spray system shall be provided for coupling transformer. The tapping for HVW system shall be done from nearby transformer/Reactor or any other suitable point of the main substation fire-fighting line-

Fire protection system shall be provided in accordance with the Central Electricity Authority (Measures relating to Safety and Electric Supply) Regulations, 2023.

#### C.8.13 Air-conditioning and ventilation system for STATCOM station

The STATCOM Station shall be provided with Air conditioning system as per requirement.

#### 1) AC System (Except Valve Hall):

Air condition system shall be provided for the following rooms in the STATCOM Building:

- a. Control and Relay room
- b. Battery room
- c. Conference Room
- d. Store cum workshop
- e. Cooling system room
- f. Lobby

Capacity and quantity of the AC units shall be decided based on heat load calculation and redundancy requirement.

### 2) Air-Conditioning System for Valve hall:

Air-Conditioning shall be provided for each Valve room for maintaining the following inside conditions round the year:

DBT - 35 °C (Maximum) Relative Humidity (RH) - 60% (Maximum)

The system shall be designed for an outside ambient temperature of 50 °C. Based on the above system design and parameters for valve room the AC system shall comprise "AHU and Air-cooled DX Condensing units" with one Main and one Standby unit for each room. The system shall be designed for 24 Hours, 365 Days of the year operation to maintain the inside temperatures of the Valve Hall for proper operation of the critical equipment. The air-cooled condensing unit shall be designed for continuous duty.



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### C.9 Engineering studies

The TSP shall carry out studies as brought out in this section with a model of the STATCOM in PSSE and PSCAD and documentation of the same shall be preserved and to be submitted to CEA/CTU, as per their requirement. The objective of these studies is to verify the steady state requirement of reactive power under normal and contingent operating conditions for peak and light loads conditions in the network.

The studies shall have to be carried out for

- Peak Load
- Light Load
- Contingency Conditions

The load flow and dynamic file available with CTU shall be provided to the TSP in PSSE version 36 format. If data is not available typical data shall be assumed by TSP.

The studies should demonstrate that the STATCOM system meets all system and equipment specified performance criteria as per the specification. Engineering studies should include, but not be limited to, the studies described in subsequent subsections.

# C.9.1 System dynamic performance studies

Dynamic performance studies should verify that the STATCOM system controls the system's dynamic performance during system disturbances. Dynamic performance studies include the following:

- a. Studies verifying that the STATCOM provides adequate dynamic control to meet the system and STATCOM system performance criteria for the system conditions.
- b. Study of response time and of the STATCOM system's behavior and contribution to the system's recovery from faults.
- c. Studies to verify the operation of any supplementary controls designed to damp power oscillations following system disturbances.
- d. Studies to evaluate the interaction of the STATCOM controls with the other nearby control systems, including high-voltage direct current (HVDC) controls, generator controls, and controls of other flexible AC transmission systems (FACTS) devices

In addition to the above, relevant studies shall include the cases stated as mentioned in Annexure-I

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### C.9.2 Harmonic performance

The studies should evaluate resultant maximum harmonic levels at the STATCOM system point of common coupling (PCC), and determine maximum stresses on all STATCOM system components. The study report should include the following:

- a. Evaluation of specified system and operating conditions (refer to Clause 5) under all possible STATCOM operating conditions.
- b. Evaluation within maximum ranges of STATCOM system component tolerances (worst performance values may not occur at detuning extremes).
- c. Evaluation with maximum system voltage unbalance (refers to item 8 and item 9 in Table 3 of Clause 5).
- Evaluation of the worst case resonance condition between STATCOM system and overall system.
- e. Evaluation of possible resonant over voltages.
- f. Transformer saturation induced harmonics for component rating calculation only.
- g. Evaluation of impact considering single phase auto reclose dead time.

#### C.9.3 Electromagnetic transients, control performance, and overvoltage studies

Transient overvoltage studies should be performed with the actual control modeled to verify that the STATCOM system equipment is adequately protected against over voltages and over currents (including excessive valve recovery voltages) from power system transients resulting from switching, fault clearing events, and credible STATCOM system mal operations. Evaluation shall include the following:

- a. Study of start-up, including transformer energization, shutdown, switching coordination, and other local area network switching events
- b. Study of STATCOM system protection and protection coordination
- c. Faults on the high-voltage (HV) and MV bus (single line-to-ground, phase-to-phase, and three-phase)
- d. Faults across the VSC, capacitors, and other equipment if used.
- e. Control interaction

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#### C.9.4 Insulation coordination study

Overall insulation coordination should be verified by considering the results of 8.4 (dynamic over voltages, and fault and switching transients), including the impacts of lightning surges on the STATCOM equipment. This study should determine and verify insulation levels, clearances, and arrester placement and ratings.

#### C.9.5 Other Studies

- a) Grounding Study
- b) Protection coordination
- c) PLC/radio interference
- d) Magnetic field strength
- e) Other studies as applicable

#### C.9.6 Software simulation models

The TSP shall provide the latest following PSCAD and PSSE (36) simulation model(s) and parameters to CEA/CTU/GRID-INDIA along with detailed documentation for the purpose of future simulation to adequately represent and model the proposed STATCOM system in the respective software:

- a. Stability model. TSP should provide a detailed STATCOM system dynamics model for use in (PSCAD and PSSE) power flow and stability simulation software The model detail should be appropriate and complete for positive-sequence power system simulation and analysis that is typically performed with power flow and transient stability programs. All appropriate control features for such analysis will be modeled, and necessary documentation on the theory and use of model should be provided. Further, a generic model, benchmarked to detailed STATCOM stability model, shall also be furnished for distribution.
- b. Transients model. TSP should provide a detailed STATCOM transients model for use in PSCAD (V-5). The model detail should be appropriate and complete for the transient response calculation of the STATCOM system. All appropriate control features for such analysis will be modeled, and necessary documentation on the theory and use of model should be provided. Further, a generic model, benchmarked to detailed STATCOM transient model, shall also be furnished for distribution.

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PSS/E files may be used for developing RTDS files/ models. For simulation of STATCOM in PSS/E file (load flow and dynamic) and PSCAD (Transient) model for STATCOM is required for study. TSP will share STATCOM models with CEA, CTU and Grid-India along with detailed documentation for above study purposes and simulations. For PSS/E, both Generic and User-defined models shall be shared by the TSP with the CEA, CTU and Grid-India. Generic model (PSS/E) response shall be benchmarked with user-defined model (PSS/E and PSCAD) to the extent possible by the TSP. Generic models can be shared by the CEA, CTU and Grid-India with the concerned stakeholders/external party (ies) e. g. STUs etc. on need basis. For User Defined model, confidentiality shall be maintained by the CEA, CTU and Grid-India. For PSCAD, User Defined model shall be provided by the TSP for which confidentiality shall be maintained by the CEA, CTU and Grid-India.

Both UDM (PSCAD and PSS/E) and Generic model (PSSE) shall be provided by OEMs to CEA/CTU/GRID-INDIA without any NDA (Non-Disclosure Agreement)

#### C.9.7 Factory tests of controls

The integrated nature of the performance of the STATCOM in an electrical grid requires the following tests:

- a. The TSP should perform factory simulator system tests for integrated control and protection system to ensure the proper operation of the same. The control system should be connected to a digital simulator with adequate representation of the electrical network for various conditions. The STATCOM system controller needs to be representative of control functions, including basic controllers but inclusive of supplementary controls, firing controls, and protective functions integrated into the controllers. TSP shall submit the FAT (Factory Acceptance Test) reports of STATCOM controls to CTU/RLDC.
- b. The simulator should provide an accurate network representation including network harmonic behavior, as well as synchronous condensers, power stations, generators (with AVRs), and pump storage schemes, existing HVDC, SVCs and STATCOMs, future SVCs and STATCOMs, FSC (fixed series capacitors), and shunt reactors/capacitors/filters.

STATCOM system control function type tests on a simulator should include the following:

- Verification of each control function.
- Verification of control linearity.
- Verification of control redundancy.
- Verification of the monitoring system.

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- Verification of the protection system with reference to integrated protective functions included in the Controllers and firing controllers.
- Verification of overall system performance for minor and major system disturbances.
- Verification of processor loading of all digital controllers.
- Verification of STATCOM system parallel operation with other controls in the system and control Stability.
- Verification of control equipment performance for auxiliary power supply voltage (AC and DC) and frequency variations (AC).
- Routine production tests of all control functions, and separately of all protection functions.

#### C.10.0 VISUAL MONITORING SYSTEM FOR WATCH AND WARD OF STATCOM STATION

Visual monitoring system (VMS) for effective watch and ward of STACOM station premises covering the areas of entire switchyard, STATCOM building, Coupling Transformer, Cooling Towers and main gate, shall be provided. The TSP shall design, supply, erect, test and commission the complete system including cameras, Digital video recorder system, mounting arrangement for cameras, cables, LAN Switches, UPS and any other items/accessories required to complete the system.

Features of VMS system shall be as those specified for main substation. The number of cameras and their locations shall be decided in such a way that any location covered in the area can be scanned. The cameras shall be located in such a way to monitor at least:

- a) Coupling Transformer, Mechanically Switched Reactors (if any) and Mechanically Switched Capacitors (if any), AC filter banks (if any).
- b) STATCOM Valve Hall, Cooling System, Electrical and Mechanical Auxiliary area.
- c) Entrance to STATCOM Station.
- d) All other Major Equipment (such as CB, CT, VT, SA etc.)

The cameras can be mounted on structures, buildings or any other suitable mounting arrangement.

## C.11.0 Spares, Special Tools and Tackles

Considering STATCOM as high technology proprietary equipment of the OEM, the TSP shall ensure necessary spares are procured to maintain the necessary reliability and availability of STATCOM station. Further all necessary special tools and tackles required for erection, testing, commissioning, and maintenance of equipment shall also be taken.

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#### **Contingency Cases for STATCOM**

#### A) N-1 Contingency

#### Contingency at 765 kV level

- 1. Three Phase Fault close to 765 kV bus of Navinal (Mundra) S/s followed by tripping of one circuit of Navinal—Bhuj-II PS 765 kV D/C line (fault persisted for 100 ms)
- 2. Single Phase to Ground Fault close to 765 kV bus of Navinal (Mundra) S/s followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3-pole opening (100 ms) of the faulted line i.e. tripping one circuit of Navinal Bhuj-II PS 765 kV D/C line
- 3. Three Phase Fault close to 765 kV bus of Navinal (Mundra) S/s followed by tripping of one circuit of Navinal Lakadia 765 kV D/C line (fault persisted for 100ms)
- 4. Single Phase to Ground Fault close to 765 kV bus of Navinal (Mundra) S/s followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3-pole opening (100 ms) of the faulted line i.e. tripping one circuit of Navinal Lakadia765 kV D/C line
- 5. Three Phase Fault close to 765 kV bus of Navinal (Mundra) S/s followed by tripping of one circuit of Navinal—Bhuj PS 765 kV D/C line (fault persisted for 100ms)
- 6. Single Phase to Ground Fault close to 765 kV bus of Navinal (Mundra) S/s followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3-pole opening (100 ms) of the faulted line i.e. tripping one circuit of Navinal Bhuj PS 765 kV D/C line
- 7. Three Phase Fault close to 765 kV bus of Bhuj-II PS followed by tripping of one circuit of Bhuj-II PS Bhuj PS 765 kV D/C line (fault persisted for 100ms)
- 8. Single Phase to Ground Fault close to 765 kV bus of Bhuj-II PS followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3-pole opening (100 ms) of the faulted line i.e. tripping one circuit of Bhuj-II PS Bhuj PS 765 kV D/C line
- Three Phase Fault close to 765 kV bus of Bhuj PS followed by tripping of one circuit of KPS1 PS-Bhuj PS 765 kV D/C line (fault persisted for 100ms)
- 10. Single Phase to Ground Fault close to 765 kV bus of Bhuj PS followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3pole opening (100 ms) of the faulted line i.e. tripping one circuit of KPS1 PS – Bhuj PS 765 kV D/C line
- 11. Three Phase Fault close to 765 kV bus of Lakadia PS followed by tripping of one circuit of KPS2 PS— Lakadia PS 765 kV D/C line (fault persisted for 100ms)

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- 12. Single Phase to Ground Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3-pole opening (100 ms) of the faulted line i.e. tripping one circuit of KPS2 PS Lakadia PS 765 kV D/C line
- 13. Three Phase Fault close to 765 kV bus of Lakadia PS followed by tripping of one circuit of KPS3 PS— Lakadia PS 765 kV D/C line (fault persisted for 100ms)
- 14. Single Phase to Ground Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3-pole opening (100 ms) of the faulted line i.e. tripping one circuit of KPS3 PS Lakadia PS 765 kV D/C line
- 15. Three Phase Fault close to 765 kV bus of Lakadia PS followed by tripping of one circuit of Halvad- Lakadia PS 765 kV D/C line (fault persisted for 100ms)
- 16. Single Phase to Ground Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3pole opening (100 ms) of the faulted line i.e. tripping one circuit of Halvad-Lakadia 765 kV D/C line
- 17. Three Phase Fault close to 765 kV bus of Lakadia PS followed by tripping of one circuit of Vataman–Lakadia PS 765 kV D/C line (fault persisted for 100ms)
- 18. Single Phase to Ground Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase and unsuccessful re-closure (dead time 1 second) followed by 3pole opening (100 ms) of the faulted line i.e. tripping one circuit of Vataman— Lakadia 765 kV D/C line

## Contingency at 400 kV level (Considering 400kV Sectionaliserunder closed condition as per the approved scheme)

- 19. Three Phase Fault close to 400 kV bus of Navinal (Mundra) S/s followed by tripping of one 765/400 kV ICT at Navinal S/s (fault persisted for 100ms)
- 20. Three Phase Fault close to 400 kV bus of Mundra S/s followed by tripping of 3 GW Load at Mundra S/s (fault persisted for 100ms) Load Throw over case.
- 21. TSP shall conduct contingency case(s) for demonstrating LVRT and HVRT requirements given at C.5 (Power System Characteristics) and C.6 (e) respectively.

#### B) N-1-1 Contingency

#### Contingency at 765 kV level

22. Case 1 and 2 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Navinal (Mundra) S/s followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of Navinal — Bhuj-II PS 765 kV D/C line) and successful re-closure(dead time 1 second)

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- 23. Case 3 and 4 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Navinal (Mundra) S/s followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup>ckt of Navinal Lakadia765 kV D/C line) and successful re-closure(dead time 1 second)
- 24. Case 5and6 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Navinal (Mundra) S/s followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup>ckt of Navinal Bhuj PS 765 kV D/C line) and successful re-closure(dead time 1 second)
- 25. Case 7 and 8 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Bhuj-II PS followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of Bhuj-II PS Bhuj PS 765 kV D/C line) and successful re-closure(dead time 1 second)
- 26. Case 9 and 10 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Bhuj PS followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of KPS1 PS Bhuj PS 765 kV D/C line) and successful re-closure(dead time 1 second)
- 27. Case 11and12 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of KPS2 PS- Lakadia PS 765 kV D/C line) and successful re-closure(dead time 1 second)
- 28. Case 13 and 14 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of KPS3 PS— Lakadia PS 765 kV D/C line) and successful re-closure(dead time 1 second)
- 29. Case 15and16 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of Halvad—Lakadia PS 765 kV D/C line) and successful re-closure(dead time 1 second)
- 30. Case 17 and 18 (consider as separate cases) + Single Phase Fault close to 765 kV bus of Lakadia PS followed by single pole opening (100 ms) of the faulted phase (2<sup>nd</sup> ckt of Vataman— Lakadia PS 765 kV D/C line) and successful re-closure(dead time 1 second)

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#### SPECIFIC TECHNICAL REQUIREMENTS FOR COMMUNICATION

The communication requirement shall be in accordance to CEA (Technical Standards for Communication System in Power System Operations) Regulations, 2020, CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations, 2022, CERC (Communication System for inter-State transmission of electricity) Regulations, 2017, CEA (Cyber Security in Power Sector) Guidelines, 2021, and CERC Guidelines on "Interface Requirements" 2024, all above documents as amended from time to time.

The complete ISTS communication system commissioned by TSP under the RFP shall be the asset of ISTS and shall be available for usage of ISTS requirements as suggested by CTU from time to time

The communication services viz. SCADA, VoIP, PMU, AGC and AMR (wherever applicable) have been identified as critical services and therefore shall be provisioned with 2+2 redundancy i.e. 2 channels for Main Control Centre and 2 channels for Backup Control Centre. In order to meet this requirement, suitable redundancy at port and card level need to be ensured by the TSP to avoid any single point of failure which may lead to interruption in real-time grid operation.

PMU to PDC communication (wherever required) shall be through 2 channels to the PDC (main) as there is no backup PDC at present.

Accordingly, all the hardware for communication services of station as stated above shall support dual redundancy for data transmission of station to respective main and backup RLDCs.

In order to meet the requirement for grid management and operation of substations, Transmission Service Provider (TSP) shall provide the following:

#### D.1.0 Navinal (Mundra) (GIS) - Bhuj 765 kV D/C line.

On Navinal (Mundra) (GIS) – Bhuj 765 kV D/C line, TSP shall supply, install and commission One (1) no. OPGW cable containing 48 Fibres (48F) on one E/W peak and conventional earth wire on other E/W peak. Proposed OPGW Hardware, Joint Box and other accessories shall be 48 Fiber OPGW.

The TSP shall install this OPGW from gantry of Navinal (Mundra) (GIS) up to the gantry of Bhuj with all associated hardware including Vibration Dampers, mid-way and gantry Joint Boxes (called OPGW Hardware hereafter) and finally terminate in Joint Boxes at end

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Substations. The transmission line length is **70 kms** (approx.) where repeater is not required to meet link budget requirement of **Navinal (Mundra) (GIS) – Bhuj** link.

Maintenance of OPGW Cable and OPGW Hardware shall be the responsibility of TSP.

## D.2.0 2 Nos. of 765 kV line bays (GIS) at Navinal (Mundra) (GIS) for termination of Navinal (Mundra) (GIS) – Bhuj 765 kV D/C line.

- (I) TSP shall supply, install and commission 1 no. FODP (144F or higher) alongwith panel and required Approach Cable (48F) with all associated hardware fittings from gantry tower to Bay Kiosk and from the Bay Kiosk to Control room
- (II) TSP shall supply, install and commission One STM-16 (FOTE) equipment alongwith panel/s supporting minimum three (3) directions with MSP (Multiplex Section Protection 1+1)with necessary interfaces to meet the voice and data communication requirement between Navinal (Mundra) (GIS) and Bhuj S/s. The suitable DC Power Supply and backup to be provided for communication equipment.
- (III) FOTE/FODP panel shall be installed in the new Bay Kiosk/ Switchyard Panel Room (SPR). The FOTE under present scope shall be integrated by TSP with the existing FOTE at control room of Navinal (Mundra) (GIS)S/s which shall be communicating with respective control center. TSP to provide necessary FODP sub rack / Splice trays/ Patch cords etc. and optical interfaces/equipment in the existing FOTE/FODP panels in control room for integration with the existing FOTE for onwards data transmission.

In case spare optical direction is not available in the existing FOTE at the control room, the TSP shall coordinate with station owner to reconfigure the directions in existing FOTE at control room. Alternatively, The TSP may integrate the FOTE under the present scope with existing FOTE in the nearby Kiosk connected to the control room FOTE (if available with spare direction). For this purpose, TSP shall provide necessary FODP sub rack / Splice trays/ Patch cords etc. and suitable optical interfaces/ equipment in the existing FOTE/FODP panels in another Kiosk (SPR).

- (IV) FOTE and FODP can be accommodated in same panel to optimize space.
- (V) The new communication equipment under the present scope shall be compatible for integration with existing regional level centralized NMS. The local configuration of the new communication equipment shall be the responsibility of TSP. The configuration work in the existing centralized NMS for integration of new Communication equipment shall be done by Regional ULDC Team, however all the necessary support in this regard shall be ensured by TSP.

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The maintenance of all the communication equipment and software thereof including FOTE, PMU, FODP, approach cable, DCPS alongwith Battery Bank shall be the responsibility of TSP.

## D.3.0 2 Nos. of 765 kV line bays (AIS) at Bhuj S/s for termination of Navinal (Mundra) (GIS) – Bhuj 765 kV D/C line.

- (I) TSP shall supply, install and commission 1 no. FODP (144F or higher) alongwith panel and required Approach Cable (48F) with all associated hardware fittings from gantry tower to Bay Kiosk and from the Bay Kiosk to Control room.
- (II) TSP shall supply, install and commission One STM-16 (FOTE) equipment alongwith panel/s supporting minimum three (3) directions with MSP (Multiplex Section Protection 1+1) with necessary interfaces to meet the voice and data communication requirement between Navinal (Mundra) (GIS) and Bhuj S/s. The suitable DC Power Supply and backup to be provided for communication equipment.
- (III) FOTE/FODP panel shall be installed in the new Bay Kiosk/ Switchyard Panel Room (SPR). The FOTE under present scope shall be integrated by TSP with the existing FOTE at control room of **Bhuj** S/s which shall be communicating with respective control center. TSP to provide necessary FODP sub rack / Splice trays/ Patch cords etc. and optical interfaces/equipment in the existing FOTE/FODP panels in control room for integration with the existing FOTE for onwards data transmission.

In case spare optical direction is not available in the existing FOTE at the control room, the TSP shall coordinate with station owner to reconfigure the directions in existing FOTE at control room. Alternatively, The TSP may integrate the FOTE under the present scope with existing FOTE in the nearby Kiosk connected to the control room FOTE (if available with spare direction). For this purpose, TSP shall provide necessary FODP sub rack / Splice trays/ Patch cords etc. and suitable optical interfaces/ equipment in the existing FOTE/FODP panels in another Kiosk (SPR).

- (IV) FOTE and FODP can be accommodated in same panel to optimize space.
- (V) The new communication equipment under the present scope shall be compatible for integration with existing regional level centralized NMS. The local configuration of the new communication equipment shall be the responsibility of TSP. The configuration work in the existing centralized NMS for integration of new Communication equipment shall be done by Regional ULDC Team, however all the necessary support in this regard shall be ensured by TSP.

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The maintenance of all the communication equipment and software thereof including FOTE, PMU, FODP, approach cable, DCPS alongwith Battery Bank shall be the responsibility of TSP.

## D.4.0 Specific Requirement for Phasor Measurement Units (PMUs)

TSP shall supply, install and commission required no. of Phasor Measurement Units (PMUs) PMUs at all the locations under the scope of TSP under this RFP as per CEA (Technical Standards for Construction of Electrical Plants and Electric Lines) Regulations, 2022 (alongwith all amendments if any), and all the other applicable Regulations, Standards, Guidelines issued time to time. The signal list shall be as per the Annexure-I Part-B of CERC Guidelines on "Interface Requirements" 2024. These PMUs shall be provided with GPS clock and LAN switch and shall connect with LAN switch of control room of respective substations/ generating stations with Fibre Optic cable. These PMUs shall be connected with the FOTE at Substation/generating stations for onwards data transmission to the PDC (Phasor Data Concentrator) located at respective RLDC. Configuration work in existing PDC at RLDC for new PMU integration shall be done by respective RLDC, however all the necessary support in this regard shall be ensured by TSP. The maintenance of all the PMUs and associated equipment shall be the responsibility of TSP.

Note: Existing Station owner/s to provide necessary support to integrate different equipment and applications of new extended bays with the existing substation e.g. Communication (through FOTE), Voice etc. for smooth operation and monitoring of new added grid elements.



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Proposed Communication for Transmission System for supply of power to Green Hydrogen/Ammonia manufacturing potential in Mundra area of Gujarat under Phase-I Part B1 scheme (3 GW at Navinal S/s)

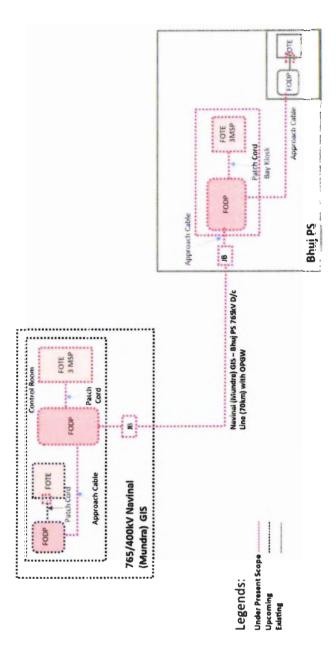


Figure F.1

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#### D.5.0 PLCC and PABX:

Power line carrier communication (PLCC) equipment complete for speech, tele-protection commands and data channels shall be provided on each transmission line. The PLCC equipment shall in brief include the following: -

- (i) Coupling device, Coupling filter line traps, carrier terminals, protection couplers, HF cables, PABX(if applicable) and maintenance and testing instruments.
- (ii) At new substation, a telephone exchange (PABX) of 24 lines shall be provided at as means of effective communication among various buildings of the substation, remote end substations and with control centers (RLDC/SLDC) etc.
- (iii) Coupling devices shall be suitable for phase to phase coupling for 400kV Transmission lines. The pass band of coupling devices shall have sufficient margin for adding communication channel in future if required. Necessary protection devices for safety of personnel and low voltage part against power frequency voltages and transient over voltage shall also be provided.
- (iv) The line traps shall be broad band tuned suitable for blocking the complete range of carrier frequencies. Line Trap shall have necessary protective devices such as lightning arresters for the protection of tuning device. Decoupling network consisting of line traps and coupling capacitors may also be required at certain substation in case of extreme frequency congestion.
- (v) The carrier terminals shall be of single side-band (SSB) amplitude modulation (AM) type and shall have 4 kHz band width. PLCC Carrier terminals and Protection couplers shall be considered for both ends of the line.
  - PLCC equipment for all the transmission lines covered under the scheme shall be provided by TSP.PLCC to be provided for following lines under present scope:

SI. No	Line name	PLCC configuration
1	Navinal (Mundra) (GIS) – Bhuj 765	1 set Analog PLCC + 1 set Digital Protection
	kV D/C line	Coupler for each circuit at both ends.

Further, CVT and Wave trap for all 765kV and 400kV line bays under present scope shall be provided by TSP.

(vi) All other associated equipment like cabling, coupling device and HF cable shall also be provided by the TSP.

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(vii) 2 sets of 48 V battery banks for PLCC and communication equipment shall be provided at each new Substation with at least 10-hour battery backup and extended backup, if required.

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#### Annexure - E

## SPECIFIC TECHNICAL REQUIREMENTS FOR INTEGRATION OF COMMUNICATION EQUIPMENT WITH REGIONAL LEVEL NMS / REGIONAL UNMS:

The new communication equipment/ system for all the substations under the present scope shall be compatible for integration with existing regional level NMS system/ Centralized Supervision and Monitoring System (CSMS) i.e. Regional UNMS. The local configuration of the new communication equipment at the station end shall be the responsibility of TSP as per **Annexure E.1**. The configuration work in the existing centralized NMS/ CSMS at Control center end, for integration of new Communication equipment/ system shall be done by Regional ULDC Team/ NMT, however all the necessary support in this regard shall be ensured by TSP.

#### Annexure E.1

#### Requirement for integration of Communication Equipment with Regional UNMS:

- TSP shall ensure that NMS/EMS/NE supplied by them is NBI compliant and all FCAPS functionality is supported in the NBI such as NE Inventory, Hardware Inventory Shelf/Slot/Card/SFP/Port, Topology, Protections, Alarms, Performance- real time and periodic, Performance KPI parameters (E-1, STM, Ethernet), Remote Configuration, Cross Connects, Trails and Circuits, Services Provisioning (NE), E-1, STM, Ethernet, TX and RS Trace, loop back and details are published in the NBI guide for the configuration parameters.
- TSP shall be obliged to provide/share all necessary documentations such as NBI Guide/MIB/IDL/WSDL/API files/ etc. for onward integration of their NMS/EMS/NE with regional UNMS.
- 3. The following support shall be provided by TSP for integration of their supplied equipment with regional UNMS:
  - Enabling and activating NBI license in their EMS/NMS and providing NBI login access along with User credentials
  - Assist in verifying NBI Connectivity with UNMS vendor for the successful communication and retrieval of data.
  - Assist in troubleshooting (if required) for NBI connectivity along with UNMS vendor for the communication and retrieval of data.
- 4. For standalone NE which is not integrated with any EMS/NMS, TSP shall provide modality of complete FCAPS data acquisition as above through industry standard programmatic methods and provide the CLI command manual.

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#### Frequently Asked Queries:

### 1.0 Transmission Line:

- Please clarify that whether shutdowns for crossing of existing transmission lines of POWERGRID/STUs/ Power Evacuation Lines from Generation Plants/ Any other Transmission Licensee will be given to TSP on chargeable basis or free of cost.
  Reply: Shutdowns for crossing of existing transmission lines of POWERGRID/ STUs/ Power Evacuation Lines from Generation Plants/ Any other Transmission Licensee will be given to
  - Evacuation Lines from Generation Plants/ Any other Transmission Licensee will be given to TSP by the concerned owner of the lines as per their own terms and conditions. As far as shutdown of ISTS lines are concerned the same can be availed by approaching respective Regional Power Committee.
- 1.2 We understand that the suggested swing angle criteria are applicable for Suspension Insulator in Suspension Tower. Further, you are requested to provide similar swing angle and clearance criteria for Pilot Insulator with Jumper and Jumper.
  - Reply: It is clarified that the swing angle criteria (as mentioned in RFP) for transmission lines is applicable for Suspension Insulator in Suspension Tower. Further, as per Clause 3.0 of Specific Technical Requirements for transmission lines, Transmission service Provider (TSP) shall adopt any additional loading/design criteria for ensuring reliability of the line, if so desired and /or deemed necessary.
- 1.3 We request you to kindly allow that use of diamond configuration at Power line crossings and the existing owner of the lines may be directed to allow the same for the successful bidders.
  - **Reply:** Power line crossing including Diamond configuration is responsibility of the TSP. TSP shall formally submit the profile of the crossing section to the owner of the existing line suggesting proposed crossing alternatives. The crossing will have to be carried out as per approval of owner of the existing line.
- 1.4 It is requested you to kindly provide present status of Forest Clearances if any transmission line corridor area falling in wildlife forest / reserve forest/ mangroves Reply: Based on the preliminary route survey, the process of initiation of forest clearance for the forest stretches, if any, enroute the proposed line alignment will be initiated by way of writing letters to the concerned authority(ies). However, it may be noted that it will be the responsibility of TSP for obtaining forest clearance for the forest stretches as provided in the survey report and also for any forest area encountered during detailed survey.

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1.5 For transmission line, no special requirement is specified for type of Insulator and creepage in RFP document. Hence it is understood that bidder can decide the type of insulator along with creepage requirement based on general CEA regulations and relevant standards. Kindly confirm.

**Reply:** The minimum specific creepage distances shall be decided for the pollution condition in the area of installation. It shall be as per CEA regulations and relevant standards.

#### 2.0 Substation

2.1 We understand that space for storage of OM spare shall be provided by existing owner within the station boundary without any cost. Kindly confirm.

Reply: Space for storage of O&M spares shall be arranged by TSP on its own.

2.2 We presume that the O&M for the end Termination bays will be in the scope of the TSP and TSP shall not be liable for any payment towards OM to the existing owner of the substation. Kindly confirm.

**Reply:** Operation and maintenance of the bays is solely responsibility of the TSP. Further, TSP shall follow CEA's "Operation and Maintenance (O&M) guidelines and Standard Format for Memorandum of Understating between New TSP and Existing TSP" issued by CEA vide its letter No. I/28514/2023 dated 22.06.2023.

- 2.3 With reference to subject scheme of existing sub-station, we assumed following scope of work:
  - (a) We assumed internal road is available and need not to consider in the present scope of work.
  - (b) Drainage is available and need not to consider in the present scope of work.
  - (c) Cable trench extension in adjacent to Main cable trench only under present scope of work.
  - (d) Levelled area being provided by developer for bay extension.

**Reply:** Regarding requirement of internal road, drainage, cable trench, leveling of the bay extension area, bidder is advised to visit site and acquaint themselves with the provisions/facilities available at substation.

- 2.4 Kindly provide the soil investigation report of soil parameters of existing substation.

  Reply: Bidder is advised to visit the substation site and ascertain the requisite parameters.
- 2.5 Kindly confirm, energy accounting of aux. power consumption. Whether it will be on

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chargeable basis or part of transmission loss.

Reply: It will be on chargeable basis.

2.6 We understand that VMS requirement is for unmanned stations only. For Manned stations VMS is not compulsory.

**Reply:** VMS shall be provided in line with requirements of RfP document.

2.7 It is understood that Construction water and power shall be provided free of cost to TSP by respective substation owner for construction of new bays.

Reply: Arrangement of construction power and water is in the scope of TSP.

2.8 It is understood that existing fire hydrant system shall be extended by the TSP for bay extension.

Reply: Existing fire hydrant system shall be extended from existing system (if required)

2.9 Please clarify that Status of land acquisition for Substations. Whether the lands have been acquired by BPC and will be transferred to TSP.

Reply: The acquisition of land for substation is in the scope of TSP.

2.10 We understood that no any dedicated metering CT and CVT required for Line/feeders. Further, we understood that requisite Energy meters for various 765 kV, 400 kV and 220 kV Feeders shall be provided and installed by CTU free of cost to TSP.

**Reply:** Dedicated metering CT and CVT are not required for line/feeders. Metering core of existing CT/CVT can be used provided accuracy class is matching with metering requirement. Requisite Special Energy Meters shall be provided and installed by CTU at the cost of TSP in C&P panel subject to space availability, else, in separate metering panel (to be provided by TSP at its cost).

2.11 A draft copy of the Connection Agreement may be furnished. A draft copy of the Connection Agreement may be furnished.

Reply: Web page link https://www.ctuil.in/formats\_gna\_transition

2.12 Please clarify whether the spare 765 kV single phase Reactor unit for Bus reactor shall be provided with 1ph 765 kV CB.

**Reply:** As per RfP, the spare 1-Ph reactor unit shall be utilized for all the bus and switchable line reactor banks (including for future reactor banks). Hence, 1ph 765 kV CB shall also be provided with spare 1-Ph reactor for utilizing with bus reactor as well as switchable line reactor.

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- 2.13 It is understood that existing busbar protection have provision for future bays and also PUs are available for future bays. BPC to confirm availability of CU and PU for bays under present scope of work at existing substations. BPC may kindly confirm availability of communication ports for integrating new PUs with the existing CUs at existing substations.
  - **Reply**: Bus Bar Protection with Central Unit (CU) is required for new bus section as specified in RfP. Peripheral Units (PUs) shall be provided by the respective bay owner. Further, augmentation/replacement of existing CU, if required, to meet the system requirement shall also be provided for proper functioning of bus bar protection.
- 2.14 For SCADA, it is understood that necessary process I/O shall be available for future bays and accordingly license for same. BPC to confirm.
  - **Reply:** Necessary process I/O along with license shall be in the scope of the successful bidder.
- 2.15 No separate FF system is envisaged under the present scope of work for existing substation. BPC to confirm.
  - **Reply:** Existing fire-fighting systems shall be extended to meet the additional requirements under present scope.
- 2.16 PLCC for 220 kV Lines are not under the scope of TSP. BPC to Confirm.It is requested to provide Type of Coupling for 220 kV Transmission Lines under present scope.
  - Reply: PLCC for 220 kV line is in the scope of developer of the line.
  - Inter circuit coupling for 220 kV D/C and phase to phase coupling for 220 kV S/C shall be applicable for PLCC.
- 2.17 BPC is requested to confirm the availability of space in the existing control rooms at existing substation for execution of extension work under current project.
  - **Reply:** Switchyard Panel Rooms are generally required for AIS type substation and relay room are required for GIS type substation. Further, if needed, control room shall be augmented as per requirement.

#### 3.0 Communication

3.1 What are the usage of OPGW, FOTE, PMU etc. under communication requirement of

**Reply**: User shall be responsible for providing compatible equipment along with appropriate interface for uninterrupted communication with the concerned control center and shall be responsible for successful integration with the communication system provided by CTU.

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Communication systems e.g. OPGW, FOTE etc. and PMU are required for grid operation through RLDC/SLDC, speech communication, tele-protection and tele-metering.

3.2 Is space for installation of communication panels are provided to TSP in existing Substations incase new bays are in the scope of TSP?

**Reply**: The space related issues are deliberated in the RfP itself. TSP to install FOTE/FODP panels in the new Bay Kiosk (Switchyard Panel Room (SPR)) / Bay Kisok/Relay Panel Room (in case of GIS S/s). Further, TSP to connect and integrate the proposed FOTE with the existing FOTE in the control room to complete communication path upto RLDC.

In Case 132 kV Substation TSP shall accommodate the said panels either by extension of existing control room or other arrangements.

3.3 How is the OPGW laying done in case of LILO lines?

Reply: In case LILO lines are on same towers (e.g. both Line in and Line Out portion are on same towers, generally done LILO of S/C lines). Then 2x48F OPGW shall berequired to install by TSP on both earthwire peak on 400 kV & 765 kV lines where two E/W peaks are available. On 220 & 132 kV lines where only one E/W peak is available TSP to install one no. 96F OPGW. Incase LILO lines are on different towers (e.g. both Line In and Line Out portion are on different towers, generally done LILO of D/C lines). Then 1x48F OPGW shall be required to install by TSP on one earthwire peak and conventional earthwire on second earthwire peak, on both Line In and Line Out portion towers of 400 kV & 765 kV lines. On 220 &132 kV lines where only one E/W peak is available TSP to install one no. 48F OPGW in place of conventional earthwire.

3.4 How is the OPGW laying done in case Multi circuit Towers?

**Reply**: In case two different lines are using common multi circuit portion for some distance (originating from different stations, may be terminating on same or on different stations). Two no. 48F OPGW to be installed on both E/W peaks for common M/C portion of 765 kV & 400 kV lines.

Incase 220/132 kV lines using multi circuit portion where single E/W peak is available one no 96F may be installed for common multi circuit portion.

3.5 How PMUs are integrated for new bays at existing Substations?

**Reply**: PMU data of new bays to be provided in the ethernet port of switch at control room and thereafter to be connected with existing FOTE of existing substation to send data to PDC of RLDC by TSP. These PMUs shall be provided with GPS clock and LAN switch and shall connect with LAN switch of control room of respective substations with Fibre Optic cable

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- 3.6 Is Spare direction available in existing FOTE for integration with new bay kiosk FOTE **Reply**: The FOTE under present scope shall be integrated by TSP with the existing FOTE at control room of substation for onwards data transmission.

  In case spare optical direction is not available in the existing FOTE at the control room, the TSP shall coordinate with station owner to reconfigure the directions in existing FOTE at control room.
- 3.7 What is the distance from LILO point to proposed substation for feasibility of repeater station?
  - **Reply**: Tentative Location of LILO point shall be as per survey report of BPC however exact location to be ascertained after detailed survey by TSP.
- 3.8 What is the make and model of existing OPGW in case LILO of main line at new substation?
  - **Reply**: All OPGW (alongwith optical fibers) meet Central Electricity Authority (Technical Standards for Communication System in Power System Operations) Regulations, 2020 and bidder shall install OPGW accordingly.
- 3.9 In case of LILO of existing line at new substation who shall provide PMUs at existing substation bays?
  - Reply: TSP to provide PMUs for all bays under their scope of RFP.

#### 4.0 Planning:

4.1 Whether the Project/ Elements are eligible for early commissioning incentive as per MoP, GoI order dated 15.07.2015.?

**Reply:** Commissioning is to be done as per the timeline mentioned in RfP. However, early commissioning shall be treated as per applicable CERC Regulations/orders.

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## Schedule: 2

## **Scheduled COD**

[Note: As referred to in the definition of "Element", "Scheduled COD", and in Articles 3.1.3 (c), 4.1 (b) and 4.3 (a) of this Agreement]

SI. No.	Name of the Transmission Element	Scheduled COD	Percentage of Quoted Transmission Charges recoverable on Scheduled COD of the Element of the Project	Element(s) which are pre-required for declaring the commercial operation (COD) of the respective Element
	Augmentation of Transformation capacity at 765/400 kV Navinal(Mundra) S/s (GIS) by 2x1500 MVA ICTs along with 2x330 MVAr, 765 kV and 2x125 MVAr, 420 kV bus reactors on Bus Section-II and 1x125 MVAr, 420 kV bus reactor on Bus Section-I. This will involve creation of 765 kV and 400 kV Bus Sections 2 through sectionalization arrangement. The 400 kV and 765 kV Sectionaliser shall be normally closed.  Navinal(Mundra) (GIS) — Bhuj 765 kV D/C line 765 kV D/C line ±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal(Mundra) (GIS) 400 kV Bus section-I	36 months from SPV transfer (20.03.2028)	100%	All Elements are required to be commissioned simultaneously as their utilization is dependent on commissioning of each other.

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SI. No.	Name of the Transmission Element	Scheduled COD	Percentage of Quoted Transmission Charges recoverable on Scheduled COD of the Element of the Project	(COD) of the
5.	±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal(Mundra) (GIS) 400 kV Bus section-II			

## Note:

- 1. Wherever required, TSP shall implement complete Dia consisting of 2(Two) Main Bays and 1(One) Tie Bay required for completion of diameter (GIS) in one-and-half breaker scheme.
- 2. TSP of Navinal (Mundra) S/s shall provide space for scope of work at SI. 1, 2, 3 (for Navinal end), 4 and 5 above.
- 3. TSP of Bhuj PS shall provide space for scope of work at Sl. 3 (for Bhuj end) above.

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#### Schedule: 3

#### **Safety Rules and Procedures**

[Note: As referred to in Articles 5.6 of this Agreement]

#### 1: Site Regulations and Safety:

The TSP shall establish Site regulations within sixty (60) days from fulfilment of conditions subsequent, as per Prudent Utility Practices setting out the rules to be observed till expiry of the Agreement at the Site and shall comply therewith.

Such Site regulations shall include, but shall not be limited to, rules in respect of security, safety of the Project, gate control, sanitation, medical care, and fire prevention, public health, environment protection, security of public life, etc.

Copies of such Site regulations shall be provided to the Nodal Agency and the CEA for the purpose of monitoring of the Project.

#### 2: Emergency Work:

In cases of any emergency, the TSP shall carry out all necessary remedial work as may be necessary.

If the work done or caused to be done by any entity, other than the TSP, the TSP shall, reimburse the actual costs incurred, to the other Party carrying out such remedial works.

#### 3: Site Clearance:

In the course of execution of the Agreement, the TSP shall keep the Site reasonably free from all unnecessary obstruction, storage, remove any surplus materials, clear away any wreckage, rubbish and temporary works from the Site, and remove any equipment no longer required for execution of the Agreement. After completion of all Elements of the Project, the TSP shall clear away and remove all wreckage, rubbish and debris of any kind from the Site, and shall leave the Site clean and safe.

#### 4: Watching and Lighting:

The TSP shall provide and maintain at its own expense all lighting, fencing, and watching when and where necessary for the proper construction, operation, maintenance / repair of any of the Elements of the Project, or for the safety of the owners and occupiers of adjacent property and for the safety of the public, during such maintenance / repair.

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### Schedule: 4

## **Computation of Transmission Charges**

#### 1.1 General

The Monthly Transmission Charges to be paid to the TSP for providing Transmission Service for any Contract Year during the term of the Agreement shall be computed in accordance with this Schedule and paid as per Sharing Regulations.

Illustration regarding payment of Transmission Charges under various scenarios (considering definitions of Contract Year, Expiry Date & Monthly Transmission Charges above) is as below: -

Illustration-1: In case the Project Elements achieve COD as per Schedule

Quoted Transmission Charges: Rs. 140 Million

Completion Schedule:

Element No.	Completion Schedule in Months	Scheduled CoD of the Element	Actual CoD of the Element	% Charges recoverable on Scheduled CoD of the Element
Element 1	28	1-Feb-2018	1-Feb-2018	25%
Element 2	38	1-Dec-2018	1-Dec-2018	75%

## Tariff Payable as follows:

Transmissi	on Charges for Elen	nent 1	Transmissio	n Charges for E	lement 2
1-Feb-18 to	140 X 25% X	5.65		****	0.00
31-Mar-18	((28+31)/365)				
1-Apr-18 to	140 X 25% X	23.39			0.00
30-Nov-18	(244/365)				
1-Dec-18 to		140 X 100%	X (121/365)		46.41
31-Mar-19					
2		140 X 100% X 1			
3		140 X 1	00% X 1		140
4		140 X 1	00% X 1		140
5		140 X 1	00% X 1		140
4** *** *** *** ***			·····		
36		140 X 100%	X (244/365)		93.59
(1-Apr to 30-					
Nov)					

Illustration-2: In case of extension of Scheduled COD as per Article 4.4.1 & 4.4.2 of this Agreement

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Quoted Transmission Charges: Rs. 140 Million

## Completion Schedule:

Element No.	Completion Schedule Months	<b>,</b>		Actual CoD of the Element	% Charge recoverable or Scheduled CoD o the Element
Element 1	20	1-	Feb-2018	1-Jul-2018	25%
Element 2	28	1-	Oct-2018	1-Dec-2018	75%

## Tariff Payable as follows:

Transmission Ch	arges for Element 1	Transmission	Charges for Eler	nent 2	
1-Feb-18 to	<u>-</u>	0.00			0.00
31-Mar-18					
1-Apr-18 to		0.00			0.00
30-Jun-18					
1-Jul-18 to	140 X 25% X	14.67			0.00
30-Nov-18	(153/365)				
1-Dec-18 to		140 X 100%	X (121/365)		46.41
31-Mar-19					
2		140 X 10	00% X 1		140
3		140 X 10	00% X 1		140
4		140 X 10	00% X 1		140
5		140 X 10	00% X 1		140
***************					
***************************************					
36		140 X 100%	X (244/365)		93.59
(1-Apr to 30-					
Nov)					

THE CENTRAL TRANSPORTER TO THE CENTRAL TRANSPORT

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NEW DELHI



## Illustration-3: In case of delay in achieving COD of Project & all individual Elements (COD of the Project achieved in Contract Year 1)

Quoted Transmission Charges: Rs. 140 Million

## Completion Schedule:

Element No.	Completion Schedule in Months		Actual CoD of the Element	% Charges recoverable on Scheduled CoD of the Element
Element 1	20	1-Feb-2018	1-Dec-2018	25%
Element 2	28	1-Oct-2018	1-Dec-2018	75%

## Tariff Payable as follows:

Transmission	Charges for E	lement 1	Transmission	Charges for E	lement 2
1-Feb-18 to	de co	0.00			0.00
31-Mar-18					
1-Apr-18 to		0.00			0.00
30-Sept-18					
1-Oct-18 to		0.00	1-Oct-18 to		0.00
30-Nov-18			30-Nov-18		
1-Dec-18 to		140 X 100%	X (121/365)		46.41
31-Mar-19					
2		140 X 1	.00% X 1		140
3		140 X 1	.00% X 1		140
4		140 X 1	.00% X 1		140
5		140 X 1	.00% X 1		140
····					
36		140 X 100%	X (244/365)		93.59
(1-Apr to 30-					
Nov)					

Central Transmission Utility of India Limited 186 Mundra I Transmission Limited







## Illustration-4: In case of delay in achieving COD of Project & all individual Elements (COD of the Project achieved in Contract Year other than Contact Year 1)

Quoted Transmission Charges: Rs. 140 Million

Completion Schedule:

Element No.	Completion	Scheduled CoD	Actual CoD of the	% Charges
	Schedule in	of the Element	Element	recoverable on
	Months			Scheduled CoD of
				the Element
Element 1	38	1-Oct-2019	1-May-2020	25%
Element 2	38	1-Oct-2019	1-May-2020	75%

Tariff Payment to be paid as:

Transmission	Charges for E	lement 1	Transmission Charges for Element		lement 2
1-Oct-19 to 31-Mar-20		0.00	1-Oct-19 to 31-Mar-20	• •	0.00
1-Apr-20 to 30-Apr-20	n or different Anna	0.00	1-Apr-20 to 30-Apr-20	and the second s	0.00
1-May-20 to 31-Mar-21	140 X 100% X (335/365)				128.49
2	140 X 100% X 1				140
3		140 X 1	00% X 1		140
4		140 X 1	00% X 1		140
5		140 X 1	00% X 1		140
***************************************					
36 (1-Apr to 30- Apr)		140 X 100%	X (30/ 365)		11.51



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## Illustration5: In case of delay in achieving COD of Element but Project COD achieved on time

Quoted Transmission Charges: Rs. 140 Million

## Completion Schedule:

Element No.	Completion Schedule in Months	Scheduled CoD of the Element	Actual CoD of the Element	% Charges recoverable on Scheduled CoD of the Element
Element 1	20	1-Feb-2018	1-Jul-2018	25%
Element 2	30	1-Dec-2018	1-Dec-2018	75%

## Tariff Payable as follows:

Transmission Charges for Element 1		Transmission Charges for Element		lement 2	
1-Feb-18 to		0.00			0.00
31-Mar-18					
1-Apr-18 to	==	0.00		-	0.00
30-Jun-18					
1-Jul-18 to	140 X 25% X	14.67			0.00
30-Nov-18	(153/365)				
1-Dec-18 to		140 X 100%	X (121/365)		46.41
31-Mar-19					
2		140 X 10	00% X 1		140
3		140 X 10	00% X 1		140
4	140 X 100% X 1				140
5		140 X 10	00% X 1		140
***************************************					
36		140 X 100% >	((244/365)		93.59
(1-Apr to 30-			•		
Nov)					

Central Transmission Utility of India Limited 188 Mundra I Transmission Limited







## Illustration-6: In case of early commissioning of Project

Quoted Transmission Charges: Rs. 140 Million

Completion Schedule:

pi				
Element No.	Completion	Scheduled CoD	Actual CoD of the	% Charges
	Schedule in	of the Element	Element	recoverable on
	Months			Scheduled CoD of
		1		the Element
Element 1	38	1-Oct-2019	1-Jul-2019	25%
Element 2	38	1-Oct-2019	1-Jul-2019	75%

## Tariff Payment to be paid as:

Transmission Charges for Element 1		Transmission Charges for Element 2		
1-July-19 to 31-Mar-20	140 X 100%	5 X (274/365)	105.09	
2	140 X 1	.00% X 1	140	
3	140 X 1	.00% X 1	140	
4	140 X 1	.00% X 1	140	
5	140 X 1	.00% X 1	140	
			5	
***************************************				
36	140 X 100%	6 X (91/365)	34.91	
(1-Apr to 30- Jun)				

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#### Illustration-7: In case of early commissioning of an element

Quoted Transmission Charges: Rs. 140 Million

Completion Schedule:

Element No.	Completion Schedule in Months	Scheduled CoD of the Element	Actual CoD of the Element	% Charges recoverable on Scheduled CoD of the Element
Element 1	38	1-Oct-2019	1-Apr-2019	25%
Element 2	38	1-Jul-2019	1-Jul-2019	75%

Tariff Payment to be paid as:

Transmission Charges for Element 1		Transmission Charges for Element 2		ement 2	
1-Apr-2019 to 30-Jun-19	140 X 25% X (91/365)	8.72	1-Apr-2019 to 30-Jun-19		0.00
1-July-19 to 31-Mar-20	140	140 X 100% X (274/ 365)			105.09
2	140 X 100% X 1				140
3	140 X 100% X 1				140
4		140 X 1	00% X 1		140
5		140 X 1	00% X 1		140
	And the second s				
36	1 /	0 V 1000	V (01 (2CE)		24.01
36 (1-Apr-30-Jun)		O X 100%	5 X (91/365)		34.91

The Transmission Charges shall be payable on monthly basis as computed above.

## 1.2 Computation of Monthly Transmission Charges

The Monthly Transmission Charges for any month m in a Contract Year n shall be calculated as below:

For AC System:

a. If Actual Transmission System Availability for the month m of contract year n is greater than or equal to 98% and less than or equal to 98.5%;

Monthly Transmission Charges MTC(m) = Tmn \*1

a. If Actual Transmission System Availability for the month m of contract year n exceeds 98.5% and less than or equal to 99.75%;

Monthly Transmission Charges MTC(m) = Tmn \* (AA/ 98.5%)

c. If Actual Transmission System Availability for the month m of contract year n is greater than 99.75%;

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Monthly Transmission Charges MTC(m) = Tmn \* (99.75% / 98.5%)

d. If Actual Transmission System Availability for the month m of contract year n is less than 98% and greater than or equal to 95.00%;

Monthly Transmission Charges MTC(m) = Tmn \* (AA/ 98%)

e. If Actual Transmission System Availability for the month m of contract year falls below 95%;

Monthly Transmission Charges MTC(m) = Tmn \* (AA/98%) - 0.02 \* (Tmn \* (AA/95%)) For DC System:

- a. If Actual Transmission System Availability for the month m of contract year n is greater than or equal to 95% and less than or equal to 96%;
  - Monthly Transmission Charges MTC(m) = Tmn \*1
- If Actual Transmission System Availability for the month m of contract year n exceeds 96% and less than or equal to 99.75%;
  - Monthly Transmission Charges MTC(m) = Tmn \* (AA/ 96%)
- c. If Actual Transmission System Availability for the month m of contract year n is greater than 99.75%;
  - Monthly Transmission Charges MTC(m) = Tmn \* (99.75% / 96%)
- d. If Actual Transmission System Availability for the month m of contract year n is less than 95% and greater than or equal to 92.00%;
  - Monthly Transmission Charges MTC(m) = Tmn \* (AA/ 95%)
- e. If Actual Transmission System Availability for the month m of contract year falls below 92%; Monthly Transmission Charges MTC(m) = Tmn \* (AA/ 95%) 0.02 \* (Tmn \* (AA/ 92%)

#### where:

- AA is the actual Availability, as certified by RPC, as per procedure provided in Schedule
- m is the month in Contract Year 'n'
- Tmn= Transmission Charges for the month 'm' in Contract Year 'n' = (=Transmission Charge/ no. of days in the Year n)\* no. of days in month m

Provided, no Transmission Charges shall be paid during the period for which the RLDC has not allowed the operation of the Element/Project due to the failure of the TSP to operate it as per the provisions of the Grid Code.

#### 1.3 RLDC Fee & Charges

The payment of RLDC fee & charges, in accordance with relevant regulations of CERC, shall be the responsibility of the TSP.

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## Schedule: 5

## **Quoted Transmission Charges**

[Quoted Transmission Charges from Annexure - 21 of the RFP of the Selected Bidder to be inserted here]

[To be incorporated from the Bid of the Selected Bidder submitted during the e-reverse auction after its selection]

Quoted Annual Transmission Charges: Rs. 3081.73 Million

SI. No.	Name of the Transmission Element	Scheduled COD from Effective Date	Percentage of Quoted Transmission Charges recoverable on Scheduled COD of the Element of the Project	Element(s) which are pre- required for declaring the commercial operation (COD) of the respective Element
1.	Augmentation of Transformation capacity at 765/400 kV Navinal(Mundra) S/s (GIS) by 2x1500 MVA ICTs along with 2x330 MVAr, 765 kV and 2x125 MVAr, 420 kV bus reactors on Bus Section-II and 1x125 MVAr, 420 kV bus reactor on Bus Section-I. This will involve creation of 765 kV and 400 kV Bus Sections 2 through sectionalization arrangement. The 400 kV and 765 kV Sectionaliser shall be normally closed.	36 Months (20.03.2028)	100%	All Elements are required to be commissioned simultaneously as their utilization is dependent on commissioning of
2.	Navinal(Mundra) (GIS) – Bhuj 765 kV D/C line			each other.
3.	765 kV line bays at each end of Navinal(Mundra) (GIS) – Bhuj 765 kV D/C line			

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4,	±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal (Mundra) (GIS) 400 kV Bus section-I			
1				
	±300 MVAr STATCOM along with	ne vi		
	2x125 MVAr MSC and 1x125 MVAr			
	MSR at Navinal (Mundra) (GIS) 400		T LIFE TO THE TOTAL TOTA	
	kV Bus section-II			

Proportionate Transmission Charges payable for each Element of the Project:

#### Note:

- 1. Wherever required, TSP shall implement complete Dia consisting of 2(Two) Main Bays and 1(One) Tie Boy required for completion of diameter (GIS) in one-and-half breaker scheme.
- 2. TSP of Navinal (Mundra) S/s shall provide space for scope of work at Sl. 1, 2, 3 (for Navinal end), 4 and 5 above.
- 3. TSP of Bhuj PS shall pravide space for scope of work at Sl. 3 (for Bhuj end) above.

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#### Schedule: 6

# Appendix –IV to Central Electricity Regulatory Commission (Terms and Conditions of Tariff) Regulations, 2024

## Procedure for Calculation of Transmission System Availability Factor for a Month

- 1. Transmission system availability factor for nth calendar month ("TAFPn") shall be calculated by the respective transmission licensee, verified by the concerned Regional Load Dispatch Centre (RLDC) and certified by the Member-Secretary, Regional Power Committee of the region concerned, separately for each AC and HVDC transmission system and grouped according to sharing of transmission charges. In the case of the AC system, transmission System Availability shall be calculated separately for each Regional Transmission System and inter-regional transmission system. In the case of the HVDC system, transmission System Availability shall be calculated on a consolidated basis for all inter-state HVDC systems.
- 2. Transmission system availability factor for nth calendar month ("TAFPn") shall be calculated by considering the following:
  - i) AC transmission lines: Each circuit of AC transmission line shall be considered as one element:
  - ii) Inter-Connecting Transformers (ICTs): Each ICT bank (three single- phase transformers together) shall form one element;
  - iii) Static VAR Compensator (SVC): SVC, along with SVC transformer, shall form one element;
  - iv) Bus Reactors or Switchable line reactors: Each Bus Reactors or Switchable line reactors shall be considered as one element;
  - v) **HVDC Bi-pole links:** Each pole of the HVDC link, along with associated equipment at both ends, shall be considered as one element;
  - vi) HVDC back-to-back station: Each block of the HVDC back-to-back station shall be considered as one element. If the associated AC line (necessary for the transfer of inter-regional power through the HVDC back-to-back station) is not available, the HVDC back-to-back station block shall also be considered unavailable;
  - vii) Static Synchronous Compensation ("STATCOM"): Each STATCOM shall be considered as a separate element.
- 3. The Availability of the AC and HVDC portion of the Transmission system shall be calculated by considering each category of transmission elements as under:

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#### LAFPn (in %) for AC system:

Where

o Total number of AC lines.

AVo Availability of a number of AC lines

p = Total number of bus reactors switchable line reactors

AVp = Availability of p number of bus reactors/switchable line reactors

q1 \* Total number of ICTs

AVq " Availability of q number of ICTs

r Total number of SVCs

AVr Availability of r number of SVCs

u Total number of STATCOM

AVu = Availability of a number of STATCOM

#### TAFMn (in %) for HVDC System:

$$\sum\nolimits_{n=1}^{\infty} \operatorname{Cxbp} (\operatorname{act}) X \operatorname{AVxbp} + \sum\nolimits_{n=1}^{\infty} \operatorname{Cy} (\operatorname{act}) \operatorname{bth} X \operatorname{AV} \operatorname{ybth}$$

4. The availability for each category of transmission elements shall be calculated based on

W here

Cxbp(act) = Total actual operated capacity of x HVDC pole

Cxbp = Total rated capacity of x\* HVDC pole

AVxbp = Availability of xth HVDC pole

Cybtb(act) = Total actual operated capacity of yth HVDC back-to-back station block

Cybtb Total rated capacity of y HVDC back-to-back station block

AVybtb " Availability of yh HVDC back-to-back station block

s = Total no of HVDC poles

the weightage factor, total hours under consideration and non-available hours for each element of that category. The formulae for calculation of the Availability of each category of the transmission elements are as per Appendix-V. The weightage factor for each

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category of transmission elements shall be considered as under:

- (a) For each circuit of the AC line The number of sub-conductors in the line multiplied by ckt-km;
- (b) For each HVDC pole- The rated MW capacity x ckt-km;
- (c) For each ICT bank The rated MVA capacity;
- (d) For SVC- The rated MVAR capacity (inductive and capacitive);
- (e) For Bus Reactor/switchable line reactors The rated MVAR capacity;
- (f) For HVDC back-to-back stations connecting two Regional grids- Rated MW capacity of each block; and
- (g) For STATCOM Total rated MVAR Capacity.
- 5. The transmission elements under outage due to the following reasons shall be deemed to be available:
  - i. Shut down availed for maintenance of another transmission scheme or construction of new element or renovation/upgradation/additional capitalization in an existing system approved by the Commission. If the other transmission scheme belongs to the transmission licensee, the Member Secretary, RPC may restrict the deemed availability period to that considered reasonable by him for the work involved. In case of a dispute regarding deemed availability, the matter may be referred to the Chairperson, CEA, within 30 days.
  - ii. Switching off of a transmission line to restrict over-voltage and manual tripping of switched reactors as per the directions of the concerned RLDC.
  - iii. Shut down of a transmission line due to the Project(s) of NHAI, Railways and Border Road Organization, including for shifting or modification of such transmission line or any other infrastructure project approved by Ministry of Power. Member Secretary, RPC may restrict the deemed availability period to that considered reasonable by him for the work involved; Provided that apart from the deemed availability, any other costs involved in the process of such shutdown of transmission line shall not be borne by the DICs.

Provided that such deemed availability shall be considered only for the period for which DICs are not affected by the shutdown of such transmission line.

6. For the following contingencies, the outage period of transmission elements, as certified by the Member Secretary, RPC, shall be excluded from the total time of the element under the period of consideration for the following contingencies:

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- i) Outage of elements due to force majeure events beyond the control of the transmission licensee. However, whether the same outage is due to force majeure (not design failure) will be verified by the Member Secretary, RPC. A reasonable restoration time for the element shall be considered by the Member Secretary, RPC, and any additional time taken by the transmission licensee for restoration of the element beyond the reasonable time shall be treated as outage time attributable to the transmission licensee. Member Secretary, RPC may consult the transmission licensee or any expert for estimation of reasonable restoration time. Circuits restored through ERS (Emergency Restoration System) shall be considered as available;
- ii) Outage caused by grid incident/disturbance not attributable to the transmission licensee, e.g. faults in a substation or bays owned by another agency causing an outage of the transmission licensee's elements, and tripping of lines, ICTs, HVDC, etc., due to grid disturbance. However, if the element is not restored on receipt of direction from RLDC while normalizing the system following grid incident/disturbance within reasonable time, the element will be considered not available for the period of outage after issuance of RLDC's direction for restoration;
- iii) The outage period which can be excluded for the purpose of sub-clause (i) and (ii) of this clause shall be declared as under:
  - a. Maximum up to one month by the Member Secretary, RPC;
  - b. Beyond one month and up to three months after the decision at RPC;
  - c. Beyond three months by the Commission for which the transmission license shall approach the Commission along with reasons and steps taken to mitigate the outage and restoration timeline.
- 7. Time frame for certification of transmission system availability: (1) The following schedule shall be followed for certification of availability by the Member Secretary of the concerned RPC:
- Submission of outage data along with documentary proof (if any) and TAFPn calculation by Transmission Licensees to RLDC/ constituents
  - By the 5th of the following month;
  - Review of the outage data by RLDC / constituents and forward the same to respective RPC – by 20th of the month;
  - Issue of availability certificate by respective RPC by the 3rd of the next month.

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#### Appendix-V

# FORMULAE FOR CALCULATION OF AVAILABILITY OF EACH CATEGORY OF TRANSMISSION ELEMENTS

#### For AC transmission system

AVo(Availability of o no. of AC lines) = 
$$\frac{Z_{pel}^2 \text{Wi(Ti-TNA)/Ti}}{z_{pel}^2 \text{Wi}}$$

AVg(Availability of q no. of ICTs) = 
$$I_{k=1}^{q} Wk(Tk-INAk)Tk$$

$$AVp(Availability of p no, of Switched Bus reactors) = \underbrace{\frac{p}{\sum_{m=1}^{p} Wm(Tm - TNAm)Tm}}_{m=1}$$

$$AV_{xbp}(Availability of an individual HVDC pole) = \frac{(Tx-TN)}{Tx}$$

AV 15th (Availability of an individual HVDC

Back-to-back Blocks) 
$$= \frac{\langle Ty, TNAy \rangle}{Ty}$$

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### For the HVDC transmission system

For the new HVDC commissioned but not completed rwelve months:

For first 12 months: [(AVzbp or AVybb)x95% 85%], subject to a ceiling of 95%.

Where.		
0	=	Total number of AC lines:
AVo	202	Availability of o number of AC lines:
P	-	Total number of bus reactors switchable line reactors:
AVp	-	Availability of p number of bus reactors switchable line reactors;
q	-	Total number of ICTs:
AVq	=	Availability of q number of ICTs:
ſ	=	Total number of SVCs:
AVr	==	Availability of r mumber of SVCs:
U	-	Total number of STATCOM
AVu	=	Availability of u number of STATCOMs:
Wi	=	Weightage factor for ith transmission line:
M.Y.	=	Weightage factor for kth ICT:
WI	=	Weightage factors for inductive & capacitive operation of hh SVC:
Wim	=	Weightage factor for mth bus reactor:
Win	=	Weightage factor for nth STATCOM
Tt Tk. Tl	-	The total hours of ith AC line, kth ICT, Ith SVC, mth Switched Bus Reactor
Tm. Tn. Ix,		& nth STATCOM, xth HVDC pole, yth HVDC back-to-back blocks during the period under consideration (excluding time period for outages not attributed to transmission licensee for the reasons given in Para 5 of the procedure)
TNAI .TNAA		The non-availability hours (excluding the time period for outages no T <sub>NA</sub> ). T <sub>NA</sub> , attributable to transmission licensee taken as deemed

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xth HVDC pole and yth HVDC back-to-back block.





availability as T<sub>NAN</sub>, T<sub>NAN</sub>, T<sub>NAN</sub>, T<sub>NAN</sub> per Para 5 of the procedure) for i<sup>th</sup> AC line. k<sup>th</sup> ICT. I<sup>th</sup> SVC. m<sup>th</sup> Switched Bus Reactor. n<sup>th</sup> STATCOM.

## Schedule: 7

Entire Bid (both financial bid and technical bid) of the Selected Bidder to be attached here

Bid Dated 09.01.2025 and 29.01.2025 shall be an integral part of this agreement.



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## Schedule: 8

### **Contract Performance Guarantee**

(To be on non-judicial stamp paper of appropriate value as per Stamp Act relevant to place of execution. Foreign entities submitting Bids are required to follow the applicable law in their country.)

In consideration of the [Insert name of the SPV or Selected Bidder on
behalf of the TSP, or Lead Member in case of the Consortium, with address] agreeing
to undertake the obligations under the Transmission Service Agreement dated
and the other RFP Project Documents and the Nodal Agency and the PFC
Consulting Limited, agreeing to execute the RFP Project Documents with the Selected
Bidder, regarding setting up the Project, the
address of the bank issuing the guarantee and address of the head office] (hereinafter
referred to as "Guarantor Bank") hereby agrees unequivocally, irrevocably and
unconditionally to pay to(being the Nodal Agency) _at[Insert
the Place from the address of the Nodal Agency indicated in the TSA] forthwith on
demand in writing from the Nodal Agency or any Officer authorized by it in this behalf,
any amount up to and not exceeding Rupees
[Insert the amount of the bank guarantee] on behalf of M/s.
[Insert name of the Selected Bidder or SPV].
This guarantee shall be valid and binding on the Guarantor Bank up to and including
and shall not be terminable by notice or any change in the constitution
of the Bank or the term of the Transmission Service Agreement or by any other reasons
whatsoever and our liability hereunder shall not be impaired or discharged by any
extension of time or variations or alternations made, given, or agreed with or without
our knowledge or consent, by or between parties to the respective agreement.
Our liability under this Guarantee is restricted to Rs Crores (Rs.
) only. Our Guarantee shall remain in force until
0 of this Agreement]. The Nodal Agency, shall be entitled to invoke this Guarantee up
to three hundred sixty five (365) days of the last date of the validity of this Guarantee.
to three handred sixty five (505) days of the last date of the validity of this dualantee.
The Guarantor Bank hereby expressly agrees that it shall not require any proof in
addition to the written demand from (in its roles as the Nodal Agency), made
in any format, raised at the above mentioned address of the Guarantor Bank, in order
to make the said payment to Nodal Agency.
The Guarantor Bank shall make payment hereunder on first demand without
restriction or conditions and notwithstanding any objection by
[Insert name of the Selected Bidder],
or any other person. The Guarantor Bank shall not require Nodal Agency to justify the
or any other person. The Quarantor bank shall not require Rodal Agency to Justify the
at n m

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invocation of this BANK GUARANTEE, nor shall the Guarantor Bank have any recourse against Nodal Agency in respect of any payment made hereunder.

THIS BANK GUARANTEE shall be interpreted in accordance with the laws of India.

The Guarantor Bank represents that this BANK GUARANTEE has been established in such form and with such content that it is fully enforceable in accordance with its terms as against the Guarantor Bank in the manner provided herein.

THIS BANK GUARANTEE shall not be affected in any manner by reason of merger, amalgamation, restructuring, liquidation, winding up, dissolution or any other change in the constitution of the Guarantor Bank.

The Guarantor Bank acknowledges that this BANK GUARANTEE is not personal to Nodal Agency and may be assigned, in whole or in part, (whether absolutely or by way of security) by Nodal Agency to any entity to whom the Nodal Agency is entitled to assign its rights and obligations under the Transmission Service Agreement.

The Guarantor Bank hereby agrees and acknowledges that Nodal Agency shall have a right to invoke this Bank Guarantee either in part or in full, as it may deem fit.

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in witness where or:
Signature
Name:
Power of attorney No.:
For:
[Insert Name of the Bank]
Banker's Seal and Full Address, including mailing address of the Head Office





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#### Schedule: 9

## Methodology for determining the Relief Under Force Majeure Event & Change in Law during Construction Period

The relief in the form of revision in tariff due to Force Majeure Event leading to extension of Scheduled COD for a period beyond one hundred eighty (180) days and/ or Change in Law during the construction period shall be as under:

 $\Delta T = [(P \times d)] \div [1 - (1 + d)^{(-n)}]$ 

Where,

 $\Delta T$  = Change in Transmission Charges for each year

P = Sum of cumulative increase or decrease in the cost of the Project due to Change in Law and interest cost during construction corresponding to the period exceeding one hundred eighty (180) due to Force Majeure Event leading to extension of Scheduled COD for a period beyond one hundred eighty (180) days

n = number of years over which the Transmission Charges has to be paid

d = Discount rate as notified by the CERC, applicable on the Bid Deadline

The increase in Transmission Charges as stated above shall be applicable only if the value of increase in Transmission Charges as calculated above exceeds 0.30% (zero point three percent) of the quoted Transmission Charges of the TSP.





# **Annexure A10**

Form-I

## Application Form for Grant of Transmission licence

## 1. Particulars of the Applicant

SN	Particulars	Details		
i.	Name of the Applicant	Mundra   Transmission Limited		
ii.	Status	Public Limited Company		
iii.	Address	C-105, Anand Niketan, New Delhi 110021		
iv.	Name, Designation & Address of the Contact Person	Shri Prashant Kumar, Head-Regulatory & Commercial, Mundra I Transmission Limited, C/o 4th Floor South Wing, KP Epitome, Makarba, Ahmedabad, 380051		
V.	Contact Telephone No	+91 9810866555		
vi.	Fax No	079-25556601		
vii.	Email ID	prashant.kumar1@adani,com		
viii.	Place of Incorporation/ Registration	New Delhi		
ix.	Year of Incorporation/ Registration	2024		
X.	Following documents are to be enclosed			
	a) Certificate of Registration	Annexure A2		
	b) Copy of Board Resolution	Annexure A11		

# 2. Particulars of the Project for which licence is being sought:

# a) Transmission Lines:

S No	Name (end-points Location)	Voltage Class (kV)	Length (km)	Type (S/C or D/C)
1.	Navinal (Mundra) (GIS) – Bhuj 765 KV D/C Line	765 kV	73.278	D/C

## b) Sub-stations:

S No	Name (Location)	Voltage Level (s) (kV)	Transformer (Nos. and MVA capacity)	Reactive/Capacitive compensation (device with MVAR Capacity)	No. of bays
1	Navinal, Mundra	765/400 KV (GIS)	2x1500 MVA ICTs (6 nos.)	2x330 MVAr, 765 kV and 2x125 MVAr, 420 kV bus reactors on Bus Section-II and 1x125MVAr, 420 kV	765 KV (GIS) ICT bays – 2 nos. 400 KV (GIS) ICT bays – 2 nos. 765 KV (GIS) Line bays – 2 nos. 765 KV (GIS) Reactor bays – 2 nos.



				bus reactor on Bus Section-I	400 KV (GIS) Reactor bays – 3 nos. 400 KV (GIS) bays – 2 nos.
2	Bhuj End, Kutch (PGCIL)	765 KV (AIS)	-	-	765 KV (AIS) Line bays – 2 nos.

# C) Commissioning Schedule

S No.	Scope of the Transmission Scheme	Scheduled COD in months from Effective Date			
1	Augmentation of Transformation capacity at 765/400 kV Navinal(Mundra) S/s (GIS) by 2x1500 MVA ICTs along with 2x330 MVAr, 765 kV and 2x125 MVAr, 420 kV bus reactors on Bus Section-II and 1x125MVAr, 420 kV bus reactor on Bus Section-I. This will involve creation of 765 kV and 400 kV Bus Sections-2 through sectionalization arrangement. The 400 kV and 765 kV Sectionaliser shall be normally closed.  Creation of New 765 kV and 400 kV Bus Section-II  765 kV Sectionaliser – 1 Set  400 kV Sectionaliser – 1 set  765/400 kV, 1500 MVA ICT-2 Nos. (on Sec-II)  765 kV ICT bays- 2 Nos. (on Sec-II)  330 MVAr 765 kV bus reactor-2 Nos. (Sec-II)  125 MVAr 420 kV bus reactor-3 Nos. (1 No. on Sec-I and 2 Nos. on Sec-II)  765 kV reactor bay- 2 Nos. (Sec-II)	20.03.2028			
2	Navinal(Mundra) (GIS) – Bhuj 765 kV D/C line				
3	765 kV line bays at each end of Navinal(Mundra) (GIS) – Bhuj 765 kV D/C line  • 765 kV line bays-2 Nos. (AIS) (for Bhuj end)  • 765 kV line bays-2 Nos. (GIS) (for Navinal (Mundra) end) (on Sec-II)				
4	<ul> <li>±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal(Mundra) (GIS) 400 kV Bus section-I</li> <li>±300 MVAr STATCOM along with 2x125MVAr MSC and 1x125MVAr MSR</li> <li>400 kV bay - 1 No.</li> </ul>				
5	<ul> <li>±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR at Navinal(Mundra) (GIS) 400 kV Bus section-II</li> <li>±300 MVAr STATCOM along with 2x125 MVAr MSC and 1x125 MVAr MSR</li> <li>400 kV bay - 1 No.</li> </ul>				



Note:

- (1) Wherever required, TSP shall implement complete Dia consisting of 2(Two) Main Bays and 1(One) Tie Bay required for completion of diameter (GIS) in one-and-half breaker scheme.
- (2) TSP of Navinal (Mundra) S/s shall provide space for scope of work at Sl. 1, 2, 3 (for Navinal end), 4 and 5 above.
- (3) TSP of Bhuj PS shall provide space for scope of work at Sl. 3 (for Bhuj end) above.
- d) Identified Long-Term transmission customers of the Project:
  - 1. Central Transmission Utility of India Limited (Nodal Agency)
- e) Any other relevant information: Nil
- Levelized transmission charges in case of project selected through the transparent process of competitive bidding and estimated completion cost of the project in other cases: Rs 3081.73 million per annum
- 4. In case applicant has been selected in accordance with the guidelines for competitive bidding, enclose:
  - (a) Recommendation of selection by the Empowered Committee
  - (b) Evaluation report made public by the Bid Process Coordinator

Bid Evaluation Committee Certificate as furnished by BPC is enclosed as Annexure A5

5. List of documents enclosed:

## Name of the Document

- a) Certificate of Registration, MoA & AoA: Annexure A2, Annexure A3
- b) Copy of Board Resolution: Annexure A11
- c) Bid Evaluation Committee Certificate as furnished by BPC: Annexure A5

(Signature of the Applicant)

Dated: 21.03.2025 Place: Ahmedabad



## Annexure A11

CERTIFIED TRUE COPY OF THE RESOLUTION PASSED AT THE MEETING OF THE MANAGEMENT COMMITTEE OF BOARD OF DIRECTORS OF ADANI ENERGY SOLUTIONS LIMITED (FORMERLY KNOWN AS ADANI TRANSMISSION LIMITED) ("THE COMPANY") HELD ON TUESDAY, THE 27<sup>TH</sup> DAY OF AUGUST, 2024 AT ADANI CORPORATE HOUSE, SHANTIGRAM, S. G. HIGHWAY, AHMEDABAD – 382 421

"RESOLVED THAT in supersession with all earlier resolutions passed in this regard Mr. M. R. Krishna Rao, Mr. Vivek Gautam, Mr. Molay Kumar Maitra, Mr. Tanmay Vyas, Mr. Praveen Tamak, Mr. Narendra Ojha, Mr. Bhavesh Kundalia, Mr. Prashant Kumar, Mr. Naresh Desai, Mr. Afak Pothiawala, Mr. Matulya Shah and Mr. Rajesh Sirigirisetty (hereinafter referred to as "Authorised Signatories") be and are hereby severally Authorised to sign and submit petitions, affidavits, agreements, declarations, undertakings, deeds, Bills, submission of details of Bank Accounts or change of Bank Accounts and other documents in connection therewith or incidental thereto before Central Electricity Regulatory Commission (CERC), Appellate Tribunal for Electricity (APTEL), Power Grid Corporation of India Limited (PGCIL), Central Transmission Utility of India Ltd (CTUIL), Power System Operation Corporation Limited (POSOCO), Regional Power Committees and Regional Load Dispatch Centers and other regulatory authorities for and on behalf of the Company.

RESOLVED FURTHER THAT the Authorised Signatories be and are hereby further severally authorised (a) to issue notices, affidavit and other documents, communications to Long Term Transmission Customers and other Parties / agencies, including Central Transmission Utility of India Limited. and WRLDC/SRLDC (b) to file Petition, Affidavit, Notices and other documents before Regulatory Commission or other Electricity body, Appellate Tribunal for Electricity and Supreme Court for issues arising out of Transmission Service Agreement and Bulk Power Transmission Agreement, (c) to engage, appoint or remove any pleaders or advocates, and sign vakalatnamas, power of attorney for such engagement or appointment and (d) to file appeal and defend the interest of the Company."

Certified True Copy
For Adani Energy Solutions Limited
(formerly known as Adani Transmission Limited)

Jaladhi Shukla Company Secretary Membership No. F5606



Pagh III

Adani Energy Solutions Ltd (formerly known as Adani Transmission Limited) Adani Corporate House Shantigram, Near Vaishno Devi Circle, S. G. Highway, Khodiyar, Ahmedabad 382 421 Gujarat, India

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